



SPECIAL REPORT RDMR-AD-17-02

JOINT EGLIN ACOUSTICS WEEK 2013 DATA REPORT

**David A. Conner, James H. Stephenson, and
Ben W. Sim**

**Aviation Development Directorate
Aviation and Missile Research, Development,
and Engineering Center**

And

**Michael E. Watts and Eric Greenwood
NASA Langley Research Center**

And

**Charles D. Smith
Analytical Mechanical Associates, Inc.**

October 2017

**Distribution Statement A: Approved for public release; distribution is
unlimited.**



DESTRUCTION NOTICE

FOR CLASSIFIED DOCUMENTS, FOLLOW THE PROCEDURES IN DoD 5200.22-M, INDUSTRIAL SECURITY MANUAL, SECTION II-19 OR DoD 5200.1-R, INFORMATION SECURITY PROGRAM REGULATION, CHAPTER IX. FOR UNCLASSIFIED, LIMITED DOCUMENTS, DESTROY BY ANY METHOD THAT WILL PREVENT DISCLOSURE OF CONTENTS OR RECONSTRUCTION OF THE DOCUMENT.

DISCLAIMER

THE FINDINGS IN THIS REPORT ARE NOT TO BE CONSTRUED AS AN OFFICIAL DEPARTMENT OF THE ARMY POSITION UNLESS SO DESIGNATED BY OTHER AUTHORIZED DOCUMENTS.

TRADE NAMES

USE OF TRADE NAMES OR MANUFACTURERS IN THIS REPORT DOES NOT CONSTITUTE AN OFFICIAL ENDORSEMENT OR APPROVAL OF THE USE OF SUCH COMMERCIAL HARDWARE OR SOFTWARE.

| | | | | |
|--|--|--|------------------------------------|--|
| REPORT DOCUMENTATION PAGE | | | Form Approved OMB No. 0704-0188 | |
| Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503 | | | | |
| 1. AGENCY USE ONLY | | 2. REPORT DATE October 2017 | | 3. REPORT TYPE AND DATES COVERED Final |
| 4. TITLE AND SUBTITLE Joint Eglin Acoustics Week 2013 Data Report | | | | 5. FUNDING NUMBERS |
| 6. AUTHOR(S) David A. Conner, James H. Stephenson, Ben W. Sim, Michael E. Watts, Eric Greenwood, Charles D. Smith | | | | |
| 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Commander, U.S. Army Research, Development, and Engineering Command ATTN: RDMR-ADF-SE Redstone Arsenal, AL 35898-5000 National Aeronautics and Space Administration Langley Research Center Hampton, VA 23681-2199 | | | | 8. PERFORMING ORGANIZATION REPORT NUMBER SR-RDMR-AD-17-02 |
| 9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) | | | | 10. SPONSORING / MONITORING AGENCY REPORT NUMBER |
| 11. SUPPLEMENTARY NOTES | | | | |
| 12a. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution is unlimited. | | | | 12b. DISTRIBUTION CODE A |
| 13. ABSTRACT (<i>Maximum 200 Words</i>) Far-field acoustic measurements were obtained for the AH-64D, HH-60M and CV-22B at the Eglin AFB, Test Area C-72, in July/August 2013. The primary purpose for this flight test was to obtain a benchmark database of detailed acoustic source noise characteristics for the aircraft operating at typical mission gross weights over a range of typical mission operating conditions. Data were acquired for a range of steady-state level and descending flight conditions, hover, and a variety of unsteady maneuver conditions. Between 30 and 37 microphones were deployed during these tests. Vehicle position and state data, as well as weather data, were acquired simultaneously with the acoustic data. This paper describes the test aircraft, onboard instrumentation, ground instrumentation, and the data acquired. Data from this test are available upon request and review. | | | | |
| 14. SUBJECT TERMS Acoustics, Rotorcraft, Apache, Blackhawk, Osprey, Acoustics Week | | | | 15. NUMBER OF PAGES 46 |
| | | | | 16. PRICE CODE |
| 17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED | | 18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED | | 19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED |
| | | | | 20. LIMITATION OF ABSTRACT SAR |

NASA/TM-2017-219681
AMRDEC-SR-RDMR-AD-17-02



Joint Eglin Acoustics Week 2013 Data Report

David A. Conner, James H. Stephenson, and Ben W. Sim
U.S. Army Aviation & Missile Research, Development, and Engineering Center
Aviation Development Directorate, Langley Research Center, Hampton, Virginia

Michael E. Watts and Eric Greenwood
Langley Research Center, Hampton, Virginia

Charles D. Smith
Anaylitical Mechanics Associates, Inc., Hampton, Virginia

November 2017

NASA STI Program . . . in Profile

Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA scientific and technical information (STI) program plays a key part in helping NASA maintain this important role.

The NASA STI program operates under the auspices of the Agency Chief Information Officer. It collects, organizes, provides for archiving, and disseminates NASA's STI. The NASA STI program provides access to the NASA Aeronautics and Space Database and its public interface, the NASA Technical Report Server, thus providing one of the largest collections of aeronautical and space science STI in the world. Results are published in both non-NASA channels and by NASA in the NASA STI Report Series, which includes the following report types:

- **TECHNICAL PUBLICATION.** Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA counterpart of peer-reviewed formal professional papers, but having less stringent limitations on manuscript length and extent of graphic presentations.
- **TECHNICAL MEMORANDUM.** Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- **CONTRACTOR REPORT.** Scientific and technical findings by NASA-sponsored contractors and grantees.

- **CONFERENCE PUBLICATION.** Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or co-sponsored by NASA.
- **SPECIAL PUBLICATION.** Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- **TECHNICAL TRANSLATION.** English-language translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services also include creating custom thesauri, building customized databases, and organizing and publishing research results.

For more information about the NASA STI program, see the following:

- Access the NASA STI program home page at <http://www.sti.nasa.gov>
- E-mail your question via the Internet to help@sti.nasa.gov
- Fax your question to the NASA STI Help Desk at 443-757-5803
- Phone the NASA STI Help Desk at 443-757-5802
- Write to:
NASA STI Help Desk
NASA Center for AeroSpace Information
7115 Standard Drive
Hanover, MD 21076-1320

NASA/TM-2017-219681
AMRDEC-SR-RDMR-AD-17-02



Joint Eglin Acoustics Week 2013 Data Report

*David A. Conner, James H. Stephenson and Ben W. Sim
U.S. Army Aviation & Missile Research, Development, and Engineering Center
Aviation Development Directorate, Langley Research Center, Hampton, Virginia*

*Michael E. Watts and Eric Greenwood
Langley Research Center, Hampton, Virginia*

*Charles D. Smith
Analytical Mechanics Associates, Inc., Hampton, Virginia*

National Aeronautics and
Space Administration

Langley Research Center
Hampton, Virginia 23681-2199

November 2017

Acknowledgments

The test could not have been accomplished without a team of dedicated individuals. The onsite test team consisted of three NASA personnel (Michael Watts, Eric Greenwood and Benny Cheung), two U.S. Army personnel (David Conner and Ben Sim), Royce Snider from Bell Helicopter, three AMA personnel (Keith Scudder, Mike Walke and Charles Smith), and two U.S. Air Force personnel (Todd Dulle and Jeremy Brown). Numerous NASA, Bell, University of Maryland, U.S. Army and Air Force personnel also provided support before, during and after the test. The authors would like to thank them for their tireless effort, professionalism and dedication in making this test happen.

| |
|---|
| <p>The use of trademarks or names of manufacturers in this report is for accurate reporting and does not constitute an official endorsement, either expressed or implied, of such products or manufacturers by the National Aeronautics and Space Administration.</p> |
|---|

Available from:

NASA Center for AeroSpace Information
7115 Standard Drive
Hanover, MD 21076-1320
443-757-5802

Abstract

Far-field acoustic measurements were obtained for the AH-64D, HH-60M and CV-22B at the Eglin AFB, Test Area C-72, in July/August 2013. The primary purpose for this flight test was to obtain a benchmark database of detailed acoustic source noise characteristics for the aircraft operating at typical mission gross weights over a range of typical mission operating conditions. Data were acquired for a range of steady-state level and descending flight conditions, hover, and a variety of unsteady maneuver conditions. Between 30 and 37 microphones were deployed during these tests. Vehicle position and state data, as well as weather data, were acquired simultaneously with the acoustic data. This paper describes the test aircraft, onboard instrumentation, ground instrumentation, and the data acquired. Data from this test are available upon request and review.

Introduction

The Chicken Little Joint Project Office of the 46th Test Squadron at Eglin AFB sponsored Acoustics Week 2013 to provide a cost-leveraged test venue to gather developmental system performance, sensor system performance, and signature data for analysis and algorithm development. The US Army Aviation Development Directorate and the NASA Langley Research Center (LaRC) teamed with the US Army's HH-60 and AH-64 Program Management Offices and the Naval Surface Warfare Center (NSWC) to collect acoustic signature data for the AH-64D, HH-60M, and the CV-22B aircraft. The test was conducted at the Eglin AFB, Test Area C-72, in July/August 2013. The primary purpose for this flight test was to obtain a benchmark database of detailed acoustic source noise characteristics for the aircraft operating at typical mission gross weights over a range of mission operating conditions, including both steady-state flight conditions as well as unsteady maneuvers. This database can be used to predict ground noise and aural detection footprints, develop low noise operations, study helicopter source noise mechanisms during maneuvering flight, and validate NASA/Army developed acoustic detection prediction codes. These prediction codes include the Rotorcraft Noise Model (RNM) (References 1 and 2), The Advanced Acoustic Model (AAM), the Acoustic Propagation and Emulation Toolset (APET), and Fundamental Rotorcraft Acoustic Modeling from Experiments (FRAME) (Reference 3). The data acquired are available to authorized organizations with a need to know. This paper will describe the testing of these aircraft and the data available.

Test Aircraft and Onboard Measurements

Test vehicles were the AH-64D and HH-60M helicopters and the CV-22B tiltrotor aircraft. Following is a brief description of each aircraft and the onboard measurements obtained for each aircraft.

The AH-64D (Tail Number 10-05626) was configured to achieve a mission representative gross weight (Figure 1). A 4-place AGM-114 Hellfire missile rack with one dummy missile was installed on each inboard pylon mount point, rocket pods (empty) were installed on each outboard pylon mount point, and an auxiliary fuel tank (Combo Pack) was installed internally, to achieve a takeoff gross weight of approximately 18,200 pounds. The Aircraft Navigation and Tracking System (ANTS), developed by

NASA Langley, was installed to obtain vehicle position and inertial navigation data. The ANTS unit incorporates a VectorNav VN-200 Inertial Navigation System (INS) chip into a self-contained device that receives the GPS signal, processes the GPS data in conjunction with built-in sensors, calculates a Kalman-filtered aircraft state solution, and logs the solution to an SD memory card at a programmable rate of 1 to 50 Hz. The state solution contains information about the location, velocity, acceleration, attitude, and attitude rates. The GPS signal was supplied by a GPS antenna installed on the tail of the aircraft during this test specifically for the ANTS. The ANTS unit was powered by internal batteries. During this test, data were sampled continuously and uninterrupted throughout the flight day at a rate of 20 Hz. Table 1 provides a list of the AH-64D variables that were acquired during this test.

The M-model HH-60 (Tail Number 04-27001), with the new wide-chord blade that is principally characterized by its unique tapered, anhedral tips (Figure 2), was used for this test. The takeoff gross weight was approximately 16,600 pounds during this test. Vehicle position and state data were obtained from the standard onboard Integrated Vehicle Health Management System (IVHMS). Table 2 provides a list of the HH-60M variables that were acquired during this test.

The AH-64D and HH-60M helicopters used during the Acoustics Week 2013 tests were based out of the US Army Aviation Development Directorate's, Aviation Applied Technology Directorate (AATD) located at Ft. Eustis, VA. The research test pilots that flew the aircraft during these tests were also provided by AATD.

The US Air Force 413th Flight Test Squadron based at Hurlburt Field, FL provided the CV-22B tiltrotor aircraft (Tail Number 99-0021) and test pilots. The aircraft used for this test (Figure 3) was a standard vehicle with a takeoff gross weight of approximately 47,000 pounds. Onboard measurements came from a full-bus capture of four of the MIL-STD-1553 Data Bus channels – Avionics A, Avionics B, Flight Controls #1, and Flight Controls #2. A serial data stream from a NovAtel High-Precision Differential GPS Receiver was captured, as well as 4-6 video channels. All data were captured using an IRIG-106 Chapter 10 compliant recorder as the data collection system. The system had an internal time counter that was synched with UTC Time from a GPS receiver and has an accuracy of 100 nanoseconds. Table 3 provides a list of the CV-22B variables that were acquired during this test.

Experimental Setup

The Eglin remote Test Range C-72 was used for this test program. During the experiment, the aircraft were flown over a NASA deployed ground-based microphone array to measure source noise hemispheres for a range of flight conditions, including level flight, approaches, hovers, and maneuvers that are representative of typical mission operating conditions. In addition to the NASA microphones, Wyle Laboratory personnel deployed a set of microphones during the AH-64D testing. Because aircraft source noise is affected by gross weight and drag, it was desirable to ballast the aircraft, when feasible, to a typical mission gross weight and drag configuration. An overview of the test range showing the primary flight track and the locations of the microphones, weather balloon, hover points, descent target point, and the NASA command and instrumentation trailers is shown in Figure 4. Detailed descriptions of the microphone instrumentation, weather system, and flight conditions are discussed in the following sections.

Acoustic Instrumentation

Wireless Acoustic Measurement Systems (WAMS) were deployed to acquire all acoustic data obtained by during this test. With the WAMS, microphone gains are set and acoustic data acquisition is initiated and terminated wirelessly from a central command computer. The acoustic pressure-time history data are recorded on compact flash cards located within each remote unit. Upon termination of each run, sufficient data metrics and system health information are transmitted back to the command computer to assure that good data were acquired at each microphone station during the run. A typical WAMS microphone station deployment is shown in Figure 5. One-half inch prepolarized free-field response condenser microphones (B&K Model 4189) fitted with grid caps and standard 4-inch diameter windscreens were used. The microphones were mounted inverted above a 15-inch diameter round ground board, $\frac{1}{4}$ radius from the edge of the ground board, as shown in Figure 5. The spacing between the microphone diaphragm and the ground board was nominally $\frac{1}{4}$ inch. The analog microphone signals were low-pass filtered at 11,670 Hz and digitized at 25,000 Hz, then recorded on compact flash cards. Each remote unit uses a GPS receiver to acquire a common time code for synchronization of the acoustic data with the vehicle tracking and performance data, as well as the weather data. Wyle Laboratories deployed additional microphones during the AH-64D testing only. Wyle microphones were mounted inverted above NASA provided ground boards. Wyle used one-half inch externally polarized free-field response condenser microphones (B&K Model 4190) connected to Type 2669 preamplifiers powered by GRAS 12AA amplifiers. The output signal was transmitted via RG-58 coax cable to a PXI chassis containing National Instruments model 4472 data acquisition cards that digitized the signal with a 24-bit A/D converter at 25,000 Hz. Calibration tones were recorded before and after measurements every day.

The primary NASA microphone array consisted of 22 ground-board-mounted microphones deployed in a linear array aligned perpendicular to the flight path. The precise location of all microphones, as well as the descent target and the NASA and Naval Surface Warfare Center (NSWC) hover points, are provided in Table . The reference microphone (microphone 11) is situated directly on the flight path and forms the origin of the Cartesian coordinate system used in Table 4 and subsequent analysis. The coordinate system is a right-hand Cartesian system with X along the flight track in the direction of flight, Y positive to the left of the flight path, and Z positive up. With the aircraft directly overhead of the reference microphone at an altitude of 100 feet above ground level (AGL), the microphone spacing was designed to provide approximately 10° angular resolution, up to 10° below the horizon. Additional microphones provide observer angles as small as 2.4° below the horizon as shown in Table . A secondary NASA microphone array of 7 microphones was deployed perpendicular to the flight track at 1,400 feet before the primary microphone array ($X = -1400$) to capture the aft-propagated noise during approaches to the descent target. The Wyle microphone array of 7 microphones was deployed perpendicular to the flight track at a point 1,500 feet beyond the primary microphone array ($X = 1500$) for the purpose of validating a Wyle developed process called Hotspot that attempts to predict the directionality of the highest noise levels in front of the vehicle. NASA microphone 30 was co-located with Wyle microphone 34 to validate Wyle's acoustic measurement capability.

Meteorological Instrumentation

A tethered weather balloon system (Figure 6) was used to acquire weather profiles during each day's flight testing period. The system consists of a winch-controlled tethered balloon, an instrument/telemetry pod, a ground-based receiver/data controller, and a ground-based support computer. Profiles of pressure, temperature, relative humidity, wind speed, and wind direction were acquired at altitudes up to 750 feet AGL. The weather balloon was located near the NASA Command Trailer as shown in Figure 4. In addition to the balloon mounted weather sensors, tripod mounted weather sensors (see Figure 5) measuring wind

velocity, pressure, temperature, and humidity were located near the centerline microphone for each of the three microphone arrays at a height of 5 feet AGL, and at the command trailer location at a height of 30 feet AGL.

Test Procedures and Flight Conditions Measured

Acoustic measurements are extremely sensitive to atmospheric conditions, especially wind and temperature profiles. During this test program flights began at dawn (approximately 0600 hours) when the winds are typically the lowest of the day, and were terminated when winds and thermals built to unacceptable levels (typically between 0900 and 1100). Experimental setup began each day with microphone system deployment approximately 3 hours prior to first flight. This allowed time to deploy the equipment, resolve system problems, and acquire all pretest data. The weather balloon was also deployed during this setup period, but kept below 100 feet AGL until approved by range control.

During data acquisition, the aircraft approached the microphone array from a distance great enough to allow the pilot to achieve a steady-state flight condition on the prescribed flight path (Heading 307° True, 310° Magnetic) at the prescribed airspeed prior to beginning acoustic data acquisition. The pilot provided data-on and -off radio calls when the aircraft reached prescribed ranges as defined in the next section. A hard deck of 50 feet AGL was maintained for safety, at all times. Upon completion of data acquisition each day, posttest data were acquired and all data were provided to the data reduction and analysis engineer for processing.

AH-64D Helicopter

AH-64D steady-state flight conditions tested are provided in Table while the maneuver flight conditions are provided in Table . Daily flight cards for the three test days for this vehicle are provided in Table through Table .

Steady-State Conditions

Steady-state test conditions measured for the AH-64D are provided in Table . The aircraft was flown in a steady-state condition throughout the duration of acoustic data acquisition, at the prescribed airspeed and glideslope, along the primary flight path shown in Figure 4.

For all level flyovers, the aircraft was flown at an altitude of 100 feet AGL at the reference microphone location. Data-on was called at 5000 feet before the primary microphone array ($X = -5000$) and data-off was called 6000 feet past the primary microphone array ($X = 6000$).

Approaches were flown to acquire the prescribed glideslope and airspeed at a sufficient range to be in a steady-state operating condition for one mile from the Descent Target, which was located on the flight path centerline 500 feet before the primary microphone array ($X = -500$). Approaches were flown on the prescribed glideslope, with the glideslope intersecting a point 50 feet above the descent target as shown in Figure 7. This steady-state condition was held for as long as possible throughout the approach to the point 50 feet above the Descent Target, with the pilot pulling out of the descent at the lowest possible altitude for safe flight operations or at an altitude sufficient to not burst the 50-foot hard deck, whichever came first. Data-on was called at 5000 feet out ($X = -5000$) and data-off at the point of the pullout from the steady-state condition.

It should be understood that the pilot was flying an approximate (due to instrument resolution and

accuracy) descent rate using standard cockpit instrumentation and that there was a certain amount of guesswork required given the typical wind variability with altitude. The emphasis was placed on minimizing control inputs rather than on hitting the precise descent point. Also, emphasis was placed on staying on the flight track centerline over maintaining a precise glideslope.

Hover data were acquired with the aircraft hovering at the prescribed heading and altitude over either the NASA hover point or the NSWC hover point (Figure 4). The pilot called data-on when a steady hover was achieved, and data-off was called by ground control after 60 seconds of acoustic data had been acquired.

Maneuver Conditions

AH-64D maneuver test point conditions are provided in Table . Conditions M1 – M16 were right and left turns at bank angles of 20° to 60°, airspeeds of 70 and 120 knots, and altitudes of 100 to 500 feet AGL. For all turns, the aircraft approached along the primary flight track and initiated the turns 2000 feet before the primary microphone array ($X = -2000$). The pilot called data-on 1000 feet before initiating the turn ($X = -3000$). The turn was held until the vehicle heading had changed by 90° (heading change from 307° to 037° or 217° True) at which point the pilot called data-off and terminated the run. M1 – M6 were 20° and 30° bank turns at 100 feet AGL. M7 and M8 were 120 knot right and left turns while descending at a rate of 500 feet per minute (fpm) such that the aircraft reached an altitude of 100 feet AGL when the run was terminated. The desire for the 45° and 60° bank turns (M9 – M16) was to obtain acoustic data when the turns were initiated at 300 feet AGL. However, due to safety concerns that altitude loss during the turns could exceed 250 feet, some of these turns were first flown at an initial altitude of 500 feet AGL. Also, conditions M9 – M16 were only flown after aircraft weight had been reduced by at least 1200 pounds through fuel burn.

M17 and M18 were quick stops performed along the primary flight path. The goal was to stop the aircraft as quickly as possible while not exceeding normal terrain flight maneuver operating conditions. M17 was a quick stop from 90 knots in level flight at 100 feet AGL, while M18 was a quick stop from 90 knots at a 500 fpm descent rate, ending in hover at an altitude between 50 and 100 feet AGL. For both these conditions, the deceleration from steady flight at 90 knots was initiated at $X = -2000$ feet. Data-on was called 1000 feet prior to initiating the deceleration ($X = -3000$) and data-off called once the aircraft had achieved a hover condition.

M19 and M20 were pull-up/push-over maneuvers performed along the primary flight path at 100 and 120 knots, respectively. The pull-up was initiated at $X = -2000$, with data-on called at $X = -3000$. Data-off was called at the end of the push-over, once the aircraft had established a level flight condition.

M21 was a maximum level flight acceleration maneuver. The aircraft approached along the primary flight path at 100 feet AGL and 40 knots airspeed. A maximum acceleration level flight condition was initiated at $X = -2000$ and held until the vehicle reached 140 knots airspeed. Data-on was called 5 seconds prior to initiating the acceleration and data-off was called once the vehicle reached 140 knots.

HH-60M Helicopter

The HH-60M steady-state flight conditions tested are provided in Table , and the maneuver flight conditions are provided in Table . Daily flight cards for the three test days for this vehicle are provided in Table through Table .

Steady-State Conditions

The steady-state test conditions measured for the HH-60M are provided in Table . The aircraft was flown in a steady-state condition throughout the duration of acoustic data acquisition, at the prescribed airspeed and glideslope, along the primary flight path shown in Figure 4.

For all level flyovers, the aircraft was flown at an altitude of 100 feet AGL at the reference microphone location. Data-on was called at $X = -5000$ and data-off was called at $X = 6000$.

Approaches were flown to acquire the prescribed glideslope and airspeed at a sufficient range to be in a steady-state operating condition one mile from the Descent Target, which was located on the flight path centerline 500 feet before the primary microphone array ($X = -500$). Approaches were flown on the prescribed glideslope, with the glideslope intersecting a point 50 feet above the descent target as shown in Figure 7. This steady-state condition was held for as long as possible throughout the approach to the point 50 feet above the Descent Target, with the pilot pulling out of the descent at the lowest possible altitude for safe flight operations or at an altitude that would prevent bursting the 50-foot hard deck, whichever came first. Data-on was called at $X = -5000$ and data-off at the point of the pullout from the steady-state condition.

It should be understood that the pilot was flying an approximate (due to instrument resolution and accuracy) descent rate using standard cockpit instrumentation and that there was a certain amount of guesswork required given the typical wind variability with altitude. The emphasis was placed on minimizing control inputs rather than on hitting the precise descent point. Also, emphasis was placed on staying on the flight track centerline over maintaining a precise glideslope.

Hover data were acquired with the aircraft hovering at the prescribed heading and altitude over either the NASA hover point or the NSWC hover point (Figure 4). The pilot called data-on when a steady hover was achieved and data-off was called by ground control after 60 seconds of acoustic data had been acquired.

Maneuver Conditions

HH-60M maneuver test point conditions are provided in Table . All maneuver test points were conducted at 100.5% RPM. Condition M1 is a variable glideslope, variable airspeed approach terminating in a hover at 50 feet above the Descent Target, as shown in Figure 8. The data-on call occurred at $X = -4500$ and data-off was called when a hover condition had been achieved.

Maneuver points M2 – M13 are right and left turns conducted at 100 feet AGL. M2 – M4 and M8 – M10 are 20° bank turns while M5 – M7 and M11 – M13 are 30° bank turns. For all turns, the aircraft approached along the normal flight track and initiated the turns at $X = -2000$. Data-on was called 1000 feet prior to initiating the turn. The turn was held until the vehicle heading had changed by 90° (heading change from 307° to 037° or 307° to 217° True) at which point data-off was called and the test point was terminated.

Maneuver points M14 & M15 are quick stops – the aircraft was stopped as quickly as possible while not exceeding normal terrain flight maneuver operating conditions. M14 was a quick stop from 90 knots in level flight at 100 feet AGL, while M15 was a quick stop from 90 knots on a 3° descending glideslope that terminated at an altitude between 50 and 100 feet AGL. For both these runs, the deceleration from steady flight at 90 knots was initiated 2000 feet before the primary microphone array. Data-on was called 1000 feet prior to initiating the deceleration ($X = -3000$), and data-off was called once the aircraft had achieved a hover condition.

CV-22B Tiltrotor Aircraft

All test conditions measured for the CV-22B are provided in Table ; while the daily flight cards for the two test days for this vehicle are provided in Table and Table . Note that in Table , every condition code has a unique priority, in case testing was ended abruptly. Due to adequate time on station, all test points were measured multiple times. During testing, for all test conditions except M1 and M2, the aircraft was flown in a steady-state condition throughout the duration of acoustic data acquisition, at the prescribed airspeed and glideslope, along the primary flight path shown in Figure 4. The rotors were operated at 84% Nr while in airplane mode (0° nacelle angle) unless otherwise noted in the flight cards. When the nacelle angle was set to anything other than 0° , the rotors were operated at 100% Nr.

For all level flyovers, the aircraft was flown at an altitude of 150 feet AGL at the reference microphone location. Data-on was called at $X = -7000$ and data-off was called at $X = 6000$.

Approaches were flown to acquire the prescribed glideslope and airspeed at a sufficient range to be in a steady-state operating condition for one mile from the Descent Target, which was located on the flight path centerline at $X = -500$. Approaches were flown on the prescribed glideslope, with the glideslope intersecting a point 50 feet above the descent target as shown in Figure 7. This steady-state condition was held for as long as possible throughout the approach to the point 50 feet above the Descent Target, with the pilot pulling out of the descent at the lowest possible altitude for safe flight operations or at an altitude that would not burst the 50-foot hard deck, whichever came first. Data-on was called at $X = -5000$ and data-off was called when the pilot initiated his pullout from the descent condition.

Hover data were acquired with the aircraft hovering at the prescribed heading and altitude over the prescribed hover point (Figure 4). The pilot called data-on when a steady hover was achieved and data-off was called by ground control after approximately 60 seconds of acoustic data acquisition.

Maneuver test point conditions for the CV-22B were simply transitions from cruise flight in airplane mode at 200 knots airspeed to hover. The aircraft approached along the normal flight track at 200 knots in airplane mode and one mile back from the target hover point began transitioning such that a hover condition was achieved over the target hover point. The only difference between conditions M1 and M2 is that M1 terminates in a 100-foot hover over the NASA hover point while M2 terminates in a 250-foot hover over the NSWC hover point. Data-on was called 5 seconds prior to initiating the transition from airplane mode and data-off was called once a stable hover condition had been achieved.

Data Reduction and Processing

Time-synchronized, calibrated pressure time history data from all microphones, weather data, vehicle position data and vehicle state data are available throughout the duration of all runs. Acoustic data are also available in the form of narrowband spectra and one-third-octave band spectra computed every 0.5 seconds during a run. Source noise hemispheres are available for all steady-state runs in one-third-octave band and narrowband format upon request and review.

The digital acoustic time domain data were transformed to the frequency domain using 4096-point Fast Fourier Transforms (FFTs) with a Hamming window applied. Averaged narrowband spectra were computed by averaging five 4096-point FFTs with 50% overlap, resulting in 0.4915-second data blocks. These averaged narrowband spectra were computed every 0.5 seconds for each microphone for the duration

of each flyover. The averaged narrowband spectra were then integrated to obtain one-third octave band spectra for center band frequencies from 10 Hz to 10 kHz. Source noise hemispheres have been created using the Rotorcraft Noise Model/Acoustic Re-propagation Technique (RNM/ART) methodology (Reference 1) using the measured flight track and acoustic data.

Vehicle position data have been processed for transformation into the local Cartesian coordinate system as described in the Acoustic Instrumentation section of this paper, but are also available in the original latitude, longitude, and altitude GPS data format. Vehicle state and weather data are available in the original text file format as a function of time.

Concluding Remarks

Far-field acoustic measurements were obtained for the AH-64D, HH-60M and CV-22B at the Eglin AFB, Test Area C-72, in July/August 2013. The measurements were obtained as part of the Acoustics Week 2013 test sponsored by the Chicken Little Joint Project Office of the 46 Test Squadron to gather developmental system performance, sensor system performance, and signature data for analysis and algorithm development. The US Army Aviation Development Directorate, the NASA Langley Research Center (LaRC), the US Army's HH-60 and AH-64 Program Management Offices, and the Naval Surface Warfare Center (NSWC) teamed to collect this acoustic signature data for these vehicles during the Acoustics Week 2013 tests. The primary purposes for these measurements were to obtain a benchmark database of detailed acoustic source noise characteristics for these aircraft for the prediction of ground noise footprints, to develop low noise operations, to study helicopter source noise mechanisms during maneuvering flight, and for validation of NASA/Army developed acoustic prediction codes such as RNM, AAM, APET and FRAME.

Data were obtained for the vehicles operating at typical mission gross weights over a range of typical mission operating conditions, including both steady-state flight conditions as well as unsteady maneuver operations. Details of all flight conditions measured during these tests, as well as the experimental setup, vehicle onboard measurements and flight procedures have been provided. Acoustic, weather, vehicle position and vehicle state data were acquired for each run. 37 microphones were deployed during the AH-64D tests while 30 microphones were deployed during the HH-60M and CV-22B tests. Acoustic data are also available in the form of pressure time-histories, narrowband spectra, and one-third-octave band spectra computed every 0.5 seconds during a run, and source noise semispheres in one-third-octave band and narrowband formats. Vehicle state and weather data are available in the original text file format as a function of time. Data from this test are available upon request and review.

References

1. Page, J. A., Wilmer, C. and Plotkin, K. J., "Rotorcraft Noise Model Technical Reference and User Manual (Version 7.1)," Wyle Report WR 08-04, February 2008.
2. Conner, D.A., and Page, J.A., "A Tool for Low Noise Procedures Design and Community Noise Impact Assessment: The Rotorcraft Noise Model (RNM)," Presented at Heli Japan 2002, Tochigi, Japan, November 11-13, 2002.
3. Greenwood, E., Schmitz, F.H., and Sickenberger, R.D., "A Semiempirical Noise Modeling Method for Helicopter Maneuvering Flight Operations," Journal of the American Helicopter Society, Vol. 60, No. 2, April 2015, pp. 1-13.

Table 1. Vehicle data acquired during AH-64D testing.

| Variable Name | Description | Units |
|----------------|---|-------|
| Time | GPS time of week | sec |
| Week | GPS week | week |
| Heading | Heading angle relative to true north | deg |
| Pitch | Pitch angle relative to horizon | deg |
| Roll | Roll angle relative to horizon | deg |
| Latitude | INS solution position in geodetic latitude | deg |
| Longitude | INS solution position in geodetic longitude | deg |
| Altitude | Height above ellipsoid (WGS84) | m |
| NedVelX | INS solution velocity in NED frame (North) | m/sec |
| NedVelY | INS solution velocity in NED frame (East) | m/sec |
| NedVelZ | INS solution velocity in NED frame (Down) | m/sec |
| AttUncertainty | Uncertainty in attitude estimate | deg |
| PosUncertainty | Uncertainty in position estimate | m |
| VelUncertainty | Uncertainty in velocity estimate | m/sec |

Table 2. Vehicle data acquired during HH-60M testing. Note: Units unavailable at time of publication.

| ID | Parameter Name | Ground Station Name | Units |
|----|---------------------|--|-------|
| 1 | ALTITUDE DENSITY | Density Altitude (Hd) | |
| 2 | ALTITUDE RATE | Altitude Rate | |
| 3 | AVG STATIC PRESSURE | Average Static Pressure | |
| 4 | AZIMUTH PLATFORM | Azimuth Platform | |
| 5 | BARO CORRECTED ALT | Barometric Corrected Altitude | |
| 6 | BARO CORRECTION | Barometric Correction | |
| 7 | CAS | Calibrated Airspeed | |
| 8 | COLLECTIVE DCU | Collective Position (from DCU) | |
| 9 | CORRECTED NZ | Corrected Load Factor | |
| 10 | CYCLIC LAT CAL | Cyclic Lateral Position Calibrated | |
| 11 | CYCLIC LONG DCU | Cyclic Longitudinal Position (from DCU) | |
| 12 | GROUND SPEED | Ground Speed | |
| 13 | IAS | Indicated Airspeed | |
| 14 | INT AUX 1 FUEL QTY | Internal Aux Tank 1 Fuel Quantity | |
| 15 | INT AUX 2 FUEL QTY | Internal Aux Tank 2 Fuel Quantity | |
| 16 | LAT ACCEL | Lateral Acceleration (Body) | |
| 17 | LAT ACCEL (DA) | Lateral Acceleration (Body) (Digital Accelerometer) | |
| 18 | LATITUDE | Latitude | |
| 19 | LONG ACCEL | Longitudinal Acceleration (Body) | |
| 20 | LONG ACCEL (DA) | Longitudinal Acceleration (Body) (Digital Accelerometer) | |

Table 2. Continued.

| ID | Parameter Name | Ground Station Name | Units |
|----|----------------------|------------------------------------|-------|
| 21 | LONGITUDE | Longitude | |
| 23 | MAIN TANK 1 FUEL QTY | Internal Main Tank 1 Fuel Quantity | |
| 24 | MAIN TANK 2 FUEL QTY | Internal Main Tank 2 Fuel Quantity | |
| 25 | NR | Main Rotor Speed (from DCU) | |
| 26 | OAT | Outside Air Temperature (OAT) | |
| 27 | PEDAL CALIBRATED | Pedal Position Calibrated | |
| 28 | PITCH | Pitch | |
| 29 | PITCH RATE | Pitch Rate (Body) | |
| 30 | PRESSURE ALTITUDE | Pressure Altitude | |
| 31 | RADALT | Radar Altitude | |
| 32 | RADALT RATE FILTERED | Filtered Radar Altitude Rate | |
| 33 | ROLL | Roll | |
| 34 | ROLL RATE | Roll Rate (Body) | |
| 35 | STABILATOR POSITION | Stabilator Position | |
| 36 | TAS | True Airspeed | |
| 37 | TAT | Total Air Temperature | |
| 38 | TORQUE 1 | Engine 1 Torque | |
| 39 | TORQUE 2 | Engine 2 Torque | |
| 40 | TOTAL FUEL QTY | Total Fuel Quantity | |
| 41 | Total Torque | Total Torque | |
| 42 | TRUE HEADING | True Heading | |
| 43 | TURN RATE | Turn Rate | |
| 44 | UTC DAY OF YEAR | UTC Day of Year | day |
| 45 | UTC HOUR | UTC Hour | hr |
| 46 | UTC MINUTE | UTC Minute | min |
| 47 | UTC SECOND | UTC Second | sec |
| 48 | UTC TIME FOM | UTC Time Figure of Merit | |
| 49 | UTC YEAR | UTC Year | yr |
| 50 | VELOCITY BELLY | Velocity Belly (Zb) | |
| 51 | VELOCITY DOWN | Velocity Down (Zn) | |
| 52 | VELOCITY EAST | Velocity East (Yn) | |
| 53 | VELOCITY NORTH | Velocity North (Xn) | |
| 54 | VELOCITY NOSE | Velocity Nose (Xb) | |
| 55 | VELOCITY RIGHT WING | Velocity Right Wing (Yb) | |
| 56 | VELOCITY XG | Velocity Xg (Geodetic) | |
| 57 | VELOCITY YG | Velocity Yg (Geodetic) | |
| 58 | VELOCITY ZG | Velocity Zg (Geodetic) | |
| 59 | VERT ACCEL | Vertical Acceleration (Body) | |

Table 2. Concluded.

| ID | Parameter Name | Ground Station Name | Units |
|----|------------------|--|-------|
| 60 | VERT ACCEL (ADC) | Vertical Acceleration (Body) (ADC) | |
| 61 | VERT ACCEL (DA) | Vertical Acceleration (Body) (Digital Accelerometer) | |
| 62 | WEIGHT GROSS | Weight Gross | |
| 63 | WIND DIRECTION | Wind Direction | |
| 64 | WIND VELOCITY | Wind Velocity | |
| 65 | YAW RATE | Yaw Rate (Body) | |

Table 3. Vehicle data acquired during CV-22B testing.

| Number | ID | Description | Units |
|--------|----------|----------------------------------|---------------------|
| 1 | AF1800GA | LWINS1 Acceleration X | ft/sec ² |
| 2 | AF1800HA | LWINS1 Acceleration Y | ft/sec ² |
| 3 | AF1800JA | LWINS1 Acceleration Z | ft/sec ² |
| 4 | A30200EA | DEU Baro Altitude | ft |
| 5 | AF1D00UA | LWINS1 Baro Bias | m |
| 6 | AP0C00HA | VSLED Calibration Airspeed | kts |
| 7 | AT17006A | FCC1 Elevator Position | in |
| 8 | AP01004A | VSLED Left Engine Torque | ft-lbs |
| 9 | AP03004A | VSLED Right Engine Torque | ft-lbs |
| 10 | AL12002C | FMU Left Feed Tank | lbs |
| 11 | AL12006C | FMU Left Aft JSAF Tank | lbs |
| 12 | AL12005C | FMU Left Fwd JSAF Tank | lbs |
| 13 | AL12004C | FMU Left Sponson Tank | lbs |
| 14 | AL12003C | FMU Left Wing Aux Tank | lbs |
| 15 | BL14002C | FMU Right Feed Tank | lbs |
| 16 | BL14006C | FMU Right Aft JSAF Tank | lbs |
| 17 | BL14005C | FMU Right Fwd JSAF Tank | lbs |
| 18 | VL14004C | FMU Right Sponson Tank | lbs |
| 19 | VL14003C | FMU Right Wing Aux Tank | lbs |
| 20 | AP0D00LA | VSLED Total Fuel Quantity | lbs |
| 21 | AP0D003A | VSLED Gross Weight | klbs |
| 22 | AF1T00GA | LWINS1 Ground Speed | kts |
| 23 | CF11007A | ADU1 Indicated Airspeed | kts |
| 24 | AT17009A | FCC1 Lateral Stick Position | in |
| 25 | AT17008A | FCC1 Longitudinal Stick Position | in |
| 26 | AF1H00UA | LWINS1 Latitude | deg |
| 27 | AF1H00QA | LWINS1 Longitude | deg |
| 28 | AF1H00EA | LWINS1 Magnetic Heading | deg |
| 29 | AP0C002A | VSLED Nacelle Angle | deg |
| 30 | AP0D002A | VSLED Outside Air Temperature | deg C |

Table 3. Continued.

| Number | ID | Description | Units |
|--------|----------|---------------------------------|---------|
| 31 | AT1700AA | FCC1 Directional Pedal Position | in |
| 32 | AF1H00CA | LWINS1 Pitch | deg |
| 33 | AF1H00YA | LWINS1 Pitch Rate | deg/sec |
| 34 | AF1H00AA | LWINS1 Platform Azimuth | deg |
| 35 | AP0C00JA | VSLED Pressure Altitude | ft |
| 36 | AP0C00KA | VSLED Radar Altitude | ft |
| 37 | AF1H00BA | LWINS1 Roll | deg |
| 38 | AF1H00XA | LWINS1 Roll Rate | deg/sec |
| 39 | AT15004A | FCC1 Rotor RPM | RPM |
| 40 | AP0C004A | VSLED Left Rotor Torque | ft-lbs |
| 41 | AP0C005A | VSLED Right Rotor Torque | ft-lbs |
| 42 | AP0D001A | VSLED Static Pressure | in Hg |
| 43 | AT1700BA | FCC1 Throttle Position | in |
| 44 | BA1300PA | ABIU Total Air Temperature | deg C |
| 45 | BA03004A | ABIU True Airspeed | kts |
| 46 | AF1H00DA | LWINS1 True Heading | deg |
| 47 | A30100MA | DEU Turn Rate | deg/sec |
| 48 | A91G00XB | MAGR UTC Year | year |
| 49 | A91L004A | MAGR UTC Day | day |
| 50 | A91L002A | MAGR UTC Hour | hr |
| 51 | A91L002B | MAGR UTC Minute | min |
| 52 | A91L003A | MAGR UTC Second | sec |
| 53 | A91L005A | MAGR UTC Time Figure of Merit | |
| 54 | AF1H008A | LWINS1 Velocity Down | ft/sec |
| 55 | AF1H006A | LWINS1 Velocity East | ft/sec |
| 56 | AF1H004A | LWINS1 Velocity North | ft/sec |
| 57 | AF18005A | LWINS1 Velocity X | ft/sec |
| 58 | AF18007A | LWINS1 Velocity Y | ft/sec |
| 59 | AF18009A | LWINS1 Velocity Z | ft/sec |
| 60 | AP0B00AA | VSLED Vertical Velocity | ft/sec |
| 61 | A30200FA | DEU Wind Bearing | deg |
| 62 | A30200GA | DEU Wind Speed | ft/sec |
| 63 | AF1H00ZA | LWINS1 Yaw Rate | deg/sec |

Table 4. Microphone location coordinates.

| Mic # | Latitude, deg | Longitude, deg | Ellipsoid Height, m | MSL Height, m | Distances Relative to Reference microphone | | | Angle below horizon at 100 ft. AGL, deg. |
|-------|---------------|----------------|---------------------|---------------|--|----------|--------|--|
| | | | | | X, ft | Y, ft | Z, ft | |
| 1 | 30.63281474 | -86.32190771 | 30.470 | 58.920 | -15.19 | 1446.23 | 5.74 | 3.7 |
| 2 | 30.63351281 | -86.32133916 | 32.141 | 60.591 | -4.45 | 1135.85 | 11.24 | 4.5 |
| 3 | 30.63476901 | -86.32025808 | 30.325 | 58.775 | 0.36 | 566.32 | 5.30 | 9.5 |
| 4 | 30.63540769 | -86.31969859 | 28.847 | 57.297 | 0.33 | 274.89 | 0.46 | 19.9 |
| 5 | 30.63563087 | -86.31950184 | 28.704 | 57.154 | 0.01 | 172.82 | -0.01 | 30.1 |
| 6 | 30.63574974 | -86.31939937 | 28.638 | 57.088 | 0.43 | 118.89 | -0.22 | 40.1 |
| 7 | 30.63582543 | -86.31933324 | 28.587 | 57.037 | 0.47 | 84.39 | -0.39 | 49.9 |
| 8 | 30.63588241 | -86.31928391 | 28.642 | 57.092 | 0.61 | 58.50 | -0.21 | 59.7 |
| 9 | 30.63593121 | -86.31924264 | 28.658 | 57.108 | 0.98 | 36.51 | -0.16 | 70.0 |
| 10 | 30.63596981 | -86.31920430 | 28.644 | 57.094 | -0.15 | 18.04 | -0.20 | 79.8 |
| 11 | 30.63600960 | -86.31917006 | 28.706 | 57.156 | 0.00 | 0.00 | 0.00 | 90.0 |
| 12 | 30.63604929 | -86.31913551 | 28.759 | 57.209 | 0.05 | -18.07 | 0.17 | -79.7 |
| 13 | 30.63608910 | -86.31910097 | 28.697 | 57.147 | 0.14 | -36.17 | -0.03 | -70.1 |
| 14 | 30.63613366 | -86.31905606 | 28.782 | 57.232 | -1.34 | -57.62 | 0.25 | -60.0 |
| 15 | 30.63619359 | -86.31900954 | 28.896 | 57.347 | 0.16 | -83.83 | 0.62 | -49.9 |
| 16 | 30.63627044 | -86.31894216 | 28.967 | 57.147 | 0.14 | -118.91 | 0.86 | -39.8 |
| 17 | 30.63638872 | -86.31883857 | 29.109 | 57.559 | 0.14 | -172.87 | 1.32 | -29.7 |
| 18 | 30.63661209 | -86.31864293 | 29.339 | 57.789 | 0.15 | -274.79 | 2.07 | -19.6 |
| 19 | 30.63725113 | -86.31808441 | 29.284 | 57.734 | 0.45 | -566.14 | 1.89 | -9.8 |
| 20 | 30.63857946 | -86.31690785 | 28.340 | 56.790 | -2.81 | -1174.71 | -1.23 | -4.9 |
| 21 | 30.63948795 | -86.31612418 | 25.905 | 54.355 | 0.23 | -1586.94 | -9.25 | -3.9 |
| 22 | 30.64237175 | -86.31449699 | 35.923 | 64.373 | 225.61 | -2732.08 | 23.50 | -1.6 |
| 23 | 30.63205939 | -86.31704820 | 33.517 | 61.967 | -1399.51 | 742.41 | 15.72 | 6.5 |
| 24 | 30.63304449 | -86.31618557 | 33.031 | 61.481 | -1399.46 | 292.96 | 14.14 | 16.3 |
| 25 | 30.63348246 | -86.31580193 | 32.945 | 61.395 | -1399.46 | 93.12 | 13.86 | 42.8 |
| 26 | 30.63370071 | -86.31561006 | 32.652 | 61.102 | -1399.64 | -6.60 | 12.90 | -85.7 |
| 27 | 30.63392022 | -86.31541790 | 32.417 | 60.867 | -1399.61 | -106.74 | 12.13 | -39.5 |
| 28 | 30.63435769 | -86.31503455 | 31.558 | 60.008 | -1399.65 | -306.38 | 9.31 | -16.5 |
| 29 | 30.63531242 | -86.31420457 | 30.017 | 58.467 | -1398.06 | -740.82 | 4.24 | -7.4 |
| 30 | 30.63848346 | -86.32298801 | 21.499 | 49.949 | 1500.51 | 7.68 | -23.70 | 86.4 |
| 31 | 30.63684201 | -86.32442542 | 29.007 | 57.457 | 1500.46 | 756.58 | 0.92 | 7.5 |
| 32 | 30.63738937 | -86.32394597 | 27.638 | 56.088 | 1500.44 | 506.83 | -3.56 | 11.5 |
| 33 | 30.63793654 | -86.32346780 | 23.449 | 51.899 | 1500.71 | 257.37 | -17.30 | 24.5 |
| 34 | 30.63848346 | -86.32298801 | 21.499 | 49.949 | 1500.51 | 7.68 | -23.70 | 86.4 |
| 35 | 30.63903026 | -86.32250906 | 24.984 | 53.434 | 1500.51 | -241.81 | -12.27 | -24.9 |

Table 4. Continued.

| Mic # | Latitude, deg | Longitude, deg | Ellipsoid Height, m | MSL Height, m | X, ft | Y, ft | Z, ft | Angle below horizon at 100 ft. AGL, deg. |
|------------------|---------------|----------------|---------------------|---------------|---------|---------|-------|--|
| 36 | 30.63957755 | -86.32202866 | 26.924 | 55.374 | 1500.24 | -491.72 | -5.91 | -12.2 |
| 37 | 30.64012563 | -86.32154926 | 27.170 | 55.620 | 1500.41 | -741.67 | -5.11 | -8.1 |
| Descent Target | | | | | -500 | 0 | | |
| NASA Hover Point | | | | | -100 | 0 | | |
| NSWC Hover Point | | | | | 4550 | 0 | | |

Table 5. AH-64D steady-state test conditions.

| Priority | Condition Code | KCAS | Alt, ft | Glide slope, deg | Descent rate, fpm | Comments |
|----------|----------------|------|---------|------------------|-------------------|---|
| 1 | L1 | 140 | 100 | - | - | Best dash speed |
| 1 | L2 | 120 | 100 | - | - | |
| 1 | L3 | 100 | 100 | - | - | |
| 1 | L4 | 80 | 100 | - | - | |
| 1 | L5 | 70 | 100 | - | - | best endurance/lowest pilot stress |
| 1 | L6 | 60 | 100 | - | - | |
| 3 | L7 | 40 | 100 | - | - | |
| 3 | L8 | 20 | 100 | - | - | |
| 3 | L9 | 120 | 1000 | - | - | |
| 3 | L10 | 120 | 3000 | - | - | |
| 1 | A1 | 70 | var. | 3 | 371 | acquire glide slope 1 mile from Descent Target |
| 1 | A2 | 70 | var. | 6 | 741 | acquire glide slope 1 mile from Descent Target |
| 1 | A3 | 70 | var. | 9 | 1109 | acquire glide slope 1 mile from Descent Target |
| 2 | A4 | 50 | var. | 6 | 529 | flown at 30° (approximate) side slip aimed at Descent Target |
| 2 | A5 | 70 | var. | 6 | 741 | flown at 30° (approximate) side slip aimed at Descent Target |
| 1 | A6 | 50 | var. | 3 | 265 | acquire glide slope 1 mile from Descent Target |
| 1 | A7 | 50 | var. | 6 | 529 | acquire glide slope 1 mile from Descent Target |
| 1 | A8 | 50 | var. | 9 | 792 | acquire glide slope 1 mile from Descent Target |
| 2 | A9 | 40 | var. | 6 | 423 | acquire glide slope 1 mile from Descent Target, loudest approach cond. per Bob Wagner |
| 1 | H1 | 0 | 200 | - | - | Heading 310° at NSWC hover point |
| 3 | H2 | 0 | 50 | - | - | Heading 310° at NASA hover point |
| 1 | H3 | 0 | var. | - | var. | Heading 310°, pop-up at NASA hover point from 50' hover at max collective to 100' and then drop back to 50' |
| 3 | H4 | 0 | 50 | - | - | Heading 40° at NASA hover point |

Table 6. AH-64D maneuver test conditions.

| Priority | Condition Code | KCAS | Alt, ft | Descent rate, fpm | Comments |
|----------|----------------|--------------------------------|---------|-------------------|---|
| 4 | M1 | 120 | 100 | 0 | 20° Right Bank |
| 4 | M2 | 120 | 100 | 0 | 20° Left Bank |
| 3 | M3 | 70 | 100 | 0 | 30° Right Bank |
| 3 | M4 | 70 | 100 | 0 | 30° Left Bank |
| 2 | M5 | 120 | 100 | 0 | 30° Right Bank |
| 2 | M6 | 120 | 100 | 0 | 30° Left Bank |
| 2 | M7 | 120 | var. | 500 | 30° Descending (500 fpm) right Bank |
| 2 | M8 | 120 | var. | 500 | 30° Descending (500 fpm) left Bank |
| 3 | M9 | 120 | 500 | as req'd | 45° Right Bank (after burning > 1200 lbs. fuel) |
| 3 | M10 | 120 | 300 | as req'd | 45° Right Bank (after burning > 1200 lbs. fuel) |
| 3 | M11 | Eliminated this condition code | | | |
| 3 | M12 | 120 | 300 | as req'd | 45° Left Bank (after burning > 1200 lbs. fuel) |
| 1 | M13 | 120 | 500 | as req'd | 60° Right Bank (after burning > 1200 lbs. fuel) |
| 1 | M14 | 120 | 300 | as req'd | 60° Right Bank (after burning > 1200 lbs. fuel) |
| 2 | M15 | Eliminated this condition code | | | |
| 2 | M16 | 120 | 300 | as req'd | 60° Left Bank (after burning > 1200 lbs. fuel) |
| 2 | M17 | 90-0 | 100 | 0 | Quick stop |
| 3 | M18 | 90-0 | 100 | 500 | Quick stop |
| 1 | M19 | 100 | 100 | 0 | approach level, pull up, then push over |
| 1 | M20 | 120 | 100 | 0 | approach level, pull up, then push over |
| 1 | M21 | 40-140 | 100 | 0 | max level flight acceleration |

Table 7. AH-64D flight card for 7/29/13.

| Date: 7/29/13 | | UTC=Local + 5 hours | | | Steve Paris / Pete Montrond | | | | | |
|------------------|-------------|---------------------|---------------|------------------|-----------------------------|---------|-------------|----------|----------|---|
| Aircraft: AH-64D | | Flight Number: 101 | | | CG: 205 | | GW#: 18,200 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 901 | N/A | 7:55:07 | 7:56:07 | ambient | n/a | n/a | 78.7 | 3.2 | 166 | Possible issues with Ch 21 |
| 101 | 3 | 8:09:22 | 8:10:34 | L3 | 100 | 0 | 78.5 | 3.3 | 117 | Data On call at 2 km (Overdrive 16) |
| 102 | 6 | 8:16:12 | 8:17:53 | L6 | 60 | 0 | 78.8 | 1.3 | 82 | |
| 103 | 7 | 8:20:41 | 8:23:02 | L7 | 40 | 0 | 79.9 | 3.4 | 90 | |
| 104 | 8 | 8:25:22 | 8:29:23 | L8 | 20 | 0 | 78.5 | 3.8 | 96 | |
| 105 | 5 | 8:32:34 | 8:34:17 | L5 | 70 | 0 | 79.9 | 0.5 | 93 | |
| 106 | 4 | 8:36:55 | 8:38:27 | L4 | 80 | 0 | 80.3 | 2.0 | 119 | |
| 107 | 3-1 | 8:40:46 | 8:41:59 | L3 | 100 | 0 | 79.5 | 2.2 | 48 | |
| 108 | 2 | 8:44:14 | 8:45:24 | L2 | 120 | 0 | 79.5 | 2.4 | 109 | |
| 109 | 1 | 8:47:46 | 8:48:48 | L1 | 140 | 0 | 79.8 | 4.4 | 69 | 130 KTAS actual |
| 110 | 36 | 8:52:45 | 8:53:52 | A1 | 70 | 3 | 79.0 | 2.7 | 90 | |
| 111 | 37 | 8:57:36 | 8:58:41 | A2 | 70 | 6 | 80.0 | 0.4 | 83 | |
| 112 | 38 | 9:02:38 | 9:03:40 | A3 | 70 | 9 | 81.0 | 1.2 | 77 | |
| 113 | 39 | 9:07:44 | 9:09:11 | A4 | 50 | 6 | 80.6 | 3.2 | 55 | 70-80' above target, ~30° sideslipped, Mic 30 overdrive late in run |
| 114 | 40 | 9:13:01 | 9:14:13 | A5 | 70 | 6 | 80.9 | 3.2 | 47 | jet noise observed to the north, ~30° sideslipped, 70' above target |
| 115 | 41 | 9:17:36 | 9:18:41 | A6 | 50 | 3 | 81.0 | 0.0 | 29 | |
| 116 | 42 | 9:22:15 | 9:23:31 | A7 | 50 | 6 | 81.6 | 2.4 | 44 | Wyle on radio during run |
| 117 | 43 | 9:27:46 | 9:29:39 | A8 | 50 | 9 | 81.8 | 2.7 | 25 | |
| 118 | 44 | 9:33:09 | 9:34:59 | A9 | 40 | 6 | 83.6 | 0.0 | 73 | |
| 119 | 39-1 | 9:38:31 | 9:38:48 | A4 | 50 | 6 | 82.8 | 1.7 | 113 | RUN ABORTED (Nearby Explosion at C52) |
| 120 | 39-2 | 9:41:34 | 9:42:52 | A4 | 50 | 6 | 82.0 | 2.4 | 136 | 70-80' above target, ~30° sideslipped |
| 121 | 40-1 | 9:46:39 | 9:48:02 | A5 | 70 | 6 | 83.1 | 2.4 | 117 | ~30° sideslipped |
| 122 | 42-1 | 9:51:12 | 9:52:12 | A7 | 50 | 6 | 82.2 | 1.5 | 44 | |
| 123 | 37-1 | 9:55:27 | 9:56:16 | A2 | 70 | 6 | 83.2 | 1.2 | 115 | |
| 902 | N/A | 10:02:09 | 10:03:08 | ambient | n/a | n/a | 83.6 | 0.7 | 150 | |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 8. AH-64D flight card for 7/30/16.

| Date: 7/30/13 | | UTC=Local + 5 hours | | | Steve Paris / Pete Montrond | | | | | Note: UTC time hack agrees with AATD "Watson", cards in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|-----------------------------|---------|-------------|----------|----------|---|
| Aircraft: AH-64D | | Flight Number: 102 | | | CG: 205 | | GW#: 18,200 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 903 | N/A | 10:49:21 | 10:50:21 | ambient | n/a | n/a | | | | |
| 124 | 9 | 11:37:40 | 11:39:06 | L9 | 120 | 0 | 72.0 | 0.0 | 220 | 1000 ft AGL |
| 125 | 10 | 11:42:56 | 11:44:31 | L10 | 120 | 0 | 73.2 | 0.0 | 262 | 3000 ft AGL |
| 126 | 3-2 | 11:46:57 | 11:48:35 | L3 | 100 | 0 | 72.7 | 0.3 | 262 | Request target altitude 130 AGL at run start, Mic 5 down, 15 O/D |
| 127 | 15 | 11:51:58 | 11:53:04 | M1 | 120 | 0 | 73.4 | 0.0 | 262 | Right turn 20° bank |
| 128 | 15-1 | 11:54:46 | 11:55:32 | M1 | 120 | 0 | 73.8 | 0.3 | 262 | Right turn 20° bank |
| 129 | 16 | 11:57:32 | 11:58:08 | M2 | 120 | 0 | 74.3 | 0.0 | 262 | Left turn 20° bank, Mic 5 up, poor gains |
| 130 | 19 | 12:00:23 | 12:00:57 | M5 | 120 | 0 | 74.7 | 0.0 | 262 | Right turn 30° bank |
| 131 | 17 | 12:03:45 | 12:04:13 | M3 | 70 | 0 | 74.3 | 0.0 | 200 | Right turn 30° bank |
| 132 | 19-1 | 12:06:06 | 12:06:32 | M5 | 120 | 0 | 75.0 | 0.2 | 181 | Right turn 30° bank |
| 133 | 18 | 12:08:37 | 12:09:04 | M4 | 70 | 0 | 73.5 | 0.0 | 191 | Left turn 30° bank |
| 134 | 20 | 12:11:07 | 12:11:30 | M6 | 120 | 0 | 73.9 | 0.0 | 191 | Left turn 30° bank |
| 135 | 33 | 12:15:03 | 12:15:57 | M19 | 100 | 0 | 74.8 | 0.0 | 191 | Pull-up/push-over (Mic 18 O/D) |
| 136 | 34 | 12:18:54 | 12:19:43 | M20 | 120 | 0 | 76.0 | 0.0 | 191 | Mic 18 O/D |
| 137 | 35 | 12:22:52 | 12:23:58 | M21 | 40-125 | 0 | 76.2 | 1.5 | 127 | Max level flight accel |
| 138 | 15-2 | 12:27:04 | 12:27:34 | M1 | 120 | 0 | 76.0 | 2.2 | 126 | Right turn 20° bank |
| 139 | 17-1 | 12:29:35 | 12:30:03 | M3 | 70 | 0 | 76.5 | 1.0 | 126 | Right turn 30° bank |
| 140 | 19-2 | 12:31:57 | 12:32:23 | M5 | 120 | 0 | 76.7 | 0.0 | 126 | Right turn 30° bank |
| 141 | 16-1 | 12:34:16 | 12:34:43 | M2 | 120 | 0 | 76.8 | 0.0 | 126 | Left turn 20° bank |
| 142 | 18-1 | 12:36:49 | 12:37:15 | M4 | 70 | 0 | 77.0 | 0.5 | 126 | Left turn 30° bank |
| 143 | 20-1 | 12:39:13 | 12:39:37 | M6 | 120 | 0 | 77.1 | 0.2 | 126 | Left turn 30° bank |
| 144 | 21 | 12:42:38 | 12:42:06 | M7 | 120 | 3 | 77.3 | 0.2 | 126 | Right turn 30° bank descending |
| 145 | 23 | 12:45:10 | 12:45:32 | M9 | 120 | - | 77.6 | 1.2 | 126 | Right turn 45° bank (rumble in background--jet engine?) (500 AGL) |
| 146 | 24 | 12:47:29 | 12:47:54 | M10 | 120 | - | 77.7 | 0.7 | 126 | Right turn 45° bank (300 AGL) |
| 147 | 24-1 | 12:49:49 | 12:50:11 | M10 | 120 | - | 77.4 | 1.2 | 126 | Right turn 45° bank (300 AGL) |
| 148 | 27 | 12:52:11 | 12:52:35 | M13 | 120 | - | 78.9 | 0.0 | 126 | Right turn 60° bank (500 AGL) |
| 149 | 28 | 13:00:12 | 13:00:37 | M14 | 120 | - | 78.5 | 0.5 | 126 | Right turn 60° bank (300 AGL) |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 8. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|---|
| 150 | 28-1 | 13:02:30 | 13:02:49 | M14 | 120 | - | 78.6 | 0.0 | 126 | Right turn 60° bank (300 AGL) |
| 151 | 22 | 13:04:11 | 13:05:05 | M8 | 120 | 3 | 78.0 | 0.2 | 126 | Left turn 30° bank descending |
| 152 | 26 | 13:07:25 | 13:07:44 | M12 | 120 | - | 79.0 | 1.5 | 126 | Left turn 45° bank (300 AGL) |
| 153 | 26-1 | 13:09:40 | 13:10:02 | M12 | 120 | - | 79.0 | 0.2 | 126 | Left turn 45° bank (300 AGL) |
| 154 | 30 | 13:12:14 | 13:12:34 | M16 | 120 | - | 79.1 | 0.5 | 126 | Left turn 60° bank (300 AGL), Mic 23 and 29 O/D |
| 155 | 30-1 | 13:14:24 | 13:14:46 | M16 | 120 | - | 79.2 | 1.0 | 126 | Left turn 60° bank (300 AGL), Mic 23 O/D |
| 156 | 31 | 13:16:47 | 13:17:31 | M17 | 90-0 | 0 | 79.8 | 0.0 | 126 | Quick stop to descent target (poor gains) |
| 157 | 31-1 | 13:19:50 | 13:20:35 | M17 | 90-0 | 0 | 79.6 | 1.0 | 121 | Quick stop to descent target |
| 158 | 31-2 | 13:22:27 | 13:23:04 | M17 | 90-0 | 0 | 79.8 | 0.0 | 167 | Quick stop to descent target |
| 159 | 32 | 13:25:43 | 13:26:23 | M18 | 90-0 | - | 79.5 | 0.0 | 165 | Descending quick-stop (500 fpm descent) |
| 160 | 32-1 | 13:28:24 | 13:29:12 | M18 | 90-0 | - | 80.7 | 0.5 | 165 | Descending quick-stop (500 fpm descent) |
| 161 | 11 | 13:34:07 | 13:35:41 | H1 | 0 | 0 | 80.2 | 0.0 | 165 | NSWC Hover |
| 162 | 12 | 13:40:33 | 13:41:09 | H2 | 0 | 0 | 81.2 | 0.0 | 164 | NASA Hover |
| 163 | 13 | 13:42:09 | 13:42:58 | H3 | 0 | 0 | 81.2 | 0.0 | 13 | Hover Popup |
| 164 | 13-1 | 13:43:42 | 13:44:24 | H3 | 0 | 0 | 81.6 | 0.0 | 142 | Hover Popup |
| 165 | 14 | 13:45:15 | 13:46:11 | H4 | 0 | 0 | 82.3 | 0.0 | 112 | Hover Heading 217 true |
| 166 | 1-1 | 13:49:31 | 13:50:17 | L1 | 140 | 0 | 81.8 | 2.0 | 126 | 130 KTAS actual, Mic 15, 18, 30 O/D |
| 167 | 1-2 | 13:53:17 | 13:54:04 | L1 | 140 | 0 | 80.2 | 0.0 | 154 | |
| 168 | 2-1 | 13:56:49 | 13:57:41 | L2 | 120 | 0 | 79.7 | 2.4 | 219 | overdrove mic 5 (on most points) |
| 169 | 3-3 | 14:00:22 | 14:01:24 | L3 | 100 | 0 | 79.5 | 1.7 | 215 | |
| 170 | 4-1 | 14:03:56 | 14:05:20 | L4 | 80 | 0 | 80.5 | 0.7 | 191 | |
| 171 | 3-4 | 14:07:55 | 14:08:59 | L3 | 100 | 0 | 80.0 | 2.2 | 200 | |
| 904 | N/A | 14:15:49 | 14:16:39 | ambient | n/a | n/a | 80.8 | 2.2 | 210 | |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 9. AH-64D flight card for 7/31/13.

| Date: 7/31/13 | | UTC=Local + 5 hours | | | Steve Paris / Pete Montrond | | | | | Note: Times in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|-----------------------------|---------|-------------|----------|----------|--------------------------------|
| Aircraft: AH-64D | | Flight Number: 103 | | | CG: 205 | | GW#: 18,200 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 905 | N/A | | | ambient | n/a | n/a | | | | |
| 906 | N/A | 11:21:02 | 11:22:02 | ambient | n/a | n/a | 69.4 | 0.0 | 229 | |
| 172 | 9-1 | 11:36:53 | 11:38:04 | L9 | 120 | 0 | 69.7 | 0.0 | 229 | 1000' AGL |
| 173 | 10-1 | 11:41:54 | 11:43:07 | L10 | 120 | 0 | 70.1 | 0.0 | 229 | 3000' AGL |
| 174 | 5-1 | 11:46:29 | 11:48:10 | L5 | 70 | 0 | 70.5 | 0.0 | 229 | O/D Mic 30 |
| 175 | 4-2 | 11:50:53 | 11:52:26 | L4 | 80 | 0 | 71.3 | 0.0 | 5 | |
| 176 | 3-5 | 11:55:10 | 11:56:28 | L3 | 100 | 0 | 72.0 | 2.7 | 329 | |
| 177 | 2-2 | 11:59:12 | 12:00:17 | L2 | 120 | 0 | 72.1 | 0.0 | 355 | |
| 178 | 1-3 | 12:03:03 | 12:04:01 | L1 | 140 | 0 | 72.3 | 0.0 | 353 | 130 KTAS actual |
| 179 | 6-1 | 12:07:07 | 12:09:03 | L6 | 60 | 0 | 72.5 | 0.0 | 353 | |
| 180 | 7-1 | 12:12:38 | 12:15:43 | L7 | 40 | 0 | 72.8 | 0.0 | 69 | |
| 181 | 8-1 | 12:19:42 | 12:24:06 | L8 | 20 | 0 | 73.0 | 0.0 | 314 | |
| 182 | 36-1 | 12:27:37 | 12:28:50 | A1 | 70 | 3 | 73.4 | 0.0 | 2 | |
| 183 | 37-1 | 12:32:26 | 12:33:28 | A2 | 70 | 6 | 73.3 | 0.0 | 2 | |
| 184 | 38-1 | 12:37:37 | 12:39:01 | A3 | 70 | 9 | 73.6 | 0.0 | 2 | |
| 185 | 41-1 | 12:42:57 | 12:44:45 | A6 | 50 | 3 | 73.2 | 0.0 | 2 | |
| 186 | 42-1 | 12:48:24 | 12:50:10 | A7 | 50 | 6 | 73.2 | 0.0 | 2 | |
| 187 | 43-1 | 12:54:10 | 12:56:04 | A8 | 50 | 9 | 74.4 | 0.0 | 99 | |
| 188 | 11-1 | 13:00:44 | 13:01:48 | H1 | 0 | 0 | 74.9 | 0.0 | 99 | NSWC Hover Point |
| 189 | 1-4 | 13:05:33 | 13:06:32 | L1 | 140 | 0 | 75.6 | 0.0 | 99 | 130 KTAS actual |
| 190 | 2-3 | 13:09:41 | 13:10:44 | L2 | 120 | 0 | 75.5 | 0.0 | 99 | |
| 191 | 3-6 | 13:13:40 | 13:14:53 | L3 | 100 | 0 | 75.3 | 0.0 | 12 | |
| 192 | 4-3 | 13:17:43 | 13:19:06 | L4 | 80 | 0 | 75.8 | 0.0 | 351 | |
| 193 | 5-2 | 13:22:04 | 13:23:42 | L5 | 70 | 0 | 76.1 | 0.0 | 99 | |
| 194 | 6-2 | 13:26:48 | 13:28:43 | L6 | 60 | 0 | 76.4 | 0.0 | 60 | |
| 195 | 33-1 | 13:31:54 | 13:32:48 | M19 | 100 | 0 | 76.4 | 0.0 | 29 | Pull-up/push-over |
| 196 | 34-1 | 13:36:13 | 13:37:11 | M20 | 120 | 0 | 76.9 | 0.7 | 181 | Pull-up/push-over |
| 197 | 35-1 | 13:40:16 | 13:42:09 | M21 | 40-140 | 0 | 77.2 | 1.7 | 180 | Max accel. |
| 198 | 24-2 | 13:47:06 | 13:47:44 | M10 | 120 | 0 | 79.1 | 0.2 | 224 | Right turn 45° bank Mic 24 O/D |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 9. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|------------------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|---|
| 199 | 28-2 | 13:49:31 | 13:50:07 | M14 | 120 | - | 78.5 | 4.6 | 210 | Right turn 60° bank many mics overdriven |
| 200 | 28-3 | 13:52:10 | 13:52:53 | M14 | 120 | - | 78.4 | 2.7 | 222 | Right turn 60° bank 25, 26 O/D |
| 201 | 28-4 | 13:55:32 | 13:56:10 | M14 | 120 | - | 79.5 | 1.0 | 217 | Right turn 60° bank |
| 202 | 26-2 | 13:58:08 | 13:58:45 | M12 | 120 | - | 78.2 | 2.0 | 237 | Left turn 45° bank Mic 15 O/D |
| 203 | 30-2 | 14:00:45 | 14:01:55 | M16 | 120 | - | 78.7 | 1.2 | 215 | Left turn 60° bank |
| 204 | 31-3 | 14:04:53 | 14:06:08 | M17 | 90-0 | 0 | 78.6 | 2.9 | 211 | Quick stop |
| 205 | 32-2 | 14:08:34 | 14:10:11 | M18 | 90-0 | - | 79.0 | 0.2 | 238 | Descending quick stop (500 fpm descent) |
| 206 | 12-1/ 14-1/ 13-1 | 14:12:20 | 14:15:32 | H2/ H3/ H4 | 0 | 0 | 79.0 | 2.4 | 254 | NASA hover, hover turn perpendicular to track (217), popup at perpendicular heading (217) |
| 207 | 3-7 | 14:18:44 | 14:19:59 | L3 | 100 | 0 | 78.9 | 3.4 | 243 | |
| 907 | N/A | 14:26:00 | 14:27:00 | ambient | n/a | n/a | 79.3 | 3.9 | 256 | Radio chatter during ambient |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 10. HH-60M steady-state test conditions.

| Priority | Condition Code | KCAS | % RPM | Glide slope, deg | Descent rate, fpm | Comments |
|----------|----------------|----------|-------|------------------|-------------------|---|
| 1 | L1 | Vh (145) | 100.5 | - | - | |
| 1 | L2 | 130 | 100.5 | - | - | |
| 1 | L3 | 110 | 100.5 | - | - | |
| 1 | L4 | 90 | 100.5 | - | - | |
| 1 | L5 | 70 | 100.5 | - | - | |
| 1 | L6 | 50 | 100.5 | - | - | |
| 2 | L7 | Vh (145) | 96.5 | - | - | |
| 1 | L8 | 130 | 96.5 | - | - | |
| 2 | L9 | 110 | 96.5 | - | - | |
| 2 | L10 | 90 | 96.5 | | | |
| 1 | L11 | 70 | 96.5 | | | |
| 2 | L12 | 50 | 96.5 | - | - | |
| 1 | A1 | 80 | 100.5 | 6 | 847 | |
| 1 | A2 | 80 | 100.5 | 6 | 847 | 25° nose left sideslip or 1 ball width sideslip left or right |
| 1 | A3 | 70 | 100.5 | 3 | 371 | |
| 1 | A4 | 70 | 100.5 | 6 | 741 | |
| 1 | A5 | 70 | 100.5 | 9 | 1109 | |
| 2 | A6 | 70 | 98 | 3 | 371 | |
| 1 | A7 | 70 | 98 | 6 | 741 | |
| 2 | A8 | 70 | 98 | 9 | 1109 | |
| 2 | A9 | 70 | 96.5 | 3 | 371 | |
| 1 | A10 | 70 | 96.5 | 6 | 741 | |
| 2 | A11 | 70 | 97 | 9 | 1109 | |
| 1 | A12 | 50 | 100 | 3 | 265 | |
| 1 | A13 | 50 | 100 | 6 | 529 | |
| 1 | A14 | 50 | 100 | 9 | 792 | |
| 2 | A15 | 50 | 98 | 3 | 265 | |
| 1 | A16 | 50 | 98 | 6 | 529 | |
| 2 | A17 | 50 | 98 | 9 | 792 | |
| 2 | A18 | 50 | 97 | 3 | 265 | |
| 1 | A19 | 50 | 97 | 6 | 529 | |
| 2 | A20 | 50 | 97 | 9 | 792 | |
| 1 | H1 | 0 | 100.5 | - | - | Altitude 200 feet, Heading 310°, at NSWC hover point |
| 1 | H2 | 0 | 100.5 | - | - | Altitude 50 feet, Heading 310°, at NASA hover point |
| 2 | H3 | 0 | 100.5 | - | - | Altitude 50 feet, Heading 40°, at NASA hover point |

Table 11. HH-60M maneuver test conditions.

| Priority | Condition Code | KCAS | Alt, ft | Descent FPA (°) | Comments |
|----------|----------------|-------------------|---------|-----------------|--|
| 1 | M1 | 70 to 50 to hover | var. | 9 to 0 to 6 | Ingress profile, transition from level flight to descent (see Figure 8) |
| 1 | M2 | 110 | 100 | 0 | Level flight 90° right turn at a 20° bank angle starting 2000' before primary array |
| 2 | M3 | 90 | 100 | 0 | Level flight 90° right turn at a 20° bank angle starting 2000' before primary array |
| 1 | M4 | 70 | 100 | 0 | Level flight 90° right turn at a 20° bank angle starting 2000' before primary array |
| 1 | M5 | 110 | 100 | 0 | Level flight 90° right turn at a 30° bank angle starting 2000' before primary array |
| 2 | M6 | 90 | 100 | 0 | Level flight 90° right turn at a 30° bank angle starting 2000' before primary array |
| 1 | M7 | 70 | 100 | 0 | Level flight 90° right turn at a 30° bank angle starting 2000' before primary array |
| 3 | M8 | 110 | 100 | 0 | Level flight 90° left turn at a 20° bank angle starting 2000' before primary array |
| 3 | M9 | 90 | 100 | 0 | Level flight 90° left turn at a 20° bank angle starting 2000' before primary array |
| 3 | M10 | 70 | 100 | 0 | Level flight 90° left turn at a 20° bank angle starting 2000' before primary array |
| 3 | M11 | 110 | 100 | 0 | Level flight 90° left turn at a 30° bank angle starting 2000' before primary array |
| 3 | M12 | 90 | 100 | 0 | Level flight 90° left turn at a 30° bank angle starting 2000' before primary array |
| 3 | M13 | 70 | 100 | 0 | Level flight 90° left turn at a 30° bank angle starting 2000' before primary array |
| 2 | M14 | 90-0 | 100 | 0 | Quick stop starting 2000' before primary array and ending near hover point |
| 1 | M15 | 90-0 | var. | 3 | Quick stop ending at 100 feet AGL, starting 2000' before primary array and ending near hover point |

Table 12. HH-60M flight card for 8/5/13.

| Date: 8/5/13 | | UTC=Local + 5 hours | | | LTC Evan Brown / CW3 Clark Hall | | | | | Note: Times in UTC-0 (a/c time hack agrees) |
|------------------|-------------|---------------------|---------------|------------------|---------------------------------|---------|-----------------------|----------|----------|---|
| Aircraft: HH-60M | | Flight Number: 104 | | | GW#: 16,600 ± 50 | | Fuel Start Wt #: 2377 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 908 | N/A | 12:22:25 | 12:23:28 | Ambient | n/a | n/a | 72.0 | 3.2 | 205 | car near NSWC hover point |
| 301 | 3 | 13:08:00 | 13:09:23 | L3 | 110 | 0 | 74.4 | 2.2 | 354 | Aircraft time may be 2 sec behind 100.5% Nr |
| 302 | 6 | 13:12:13 | 13:13:27 | L6 | 50 | 0 | 75.6 | 2.2 | 346 | ABORT: terminated at pilot discretion |
| 303 | 6-1 | 13:17:42 | 13:20:22 | L6 | 50 | 0 | 75.0 | 3.2 | 340 | |
| 304 | 5 | 13:23:10 | 13:24:57 | L5 | 70 | 0 | 76.1 | 1.2 | 354 | |
| 305 | 4 | 13:28:05 | 13:29:26 | L4 | 90 | 0 | 76.7 | 1.7 | 328 | |
| 306 | 3-1 | 13:32:58 | 13:34:07 | L3 | 110 | 0 | 76.7 | 2.0 | 330 | |
| 307 | 2 | 13:37:13 | 13:38:13 | L2 | 130 | 0 | 76.9 | 1.7 | 13 | |
| 308 | 1 | 13:41:35 | 13:42:26 | L1 | 145 | 0 | 77.5 | 3.4 | 329 | 152 KTAS actual |
| 309 | 12 | 13:46:08 | 13:48:29 | L12 | 50 | 0 | 78.5 | 0.2 | 338 | reduced NR (96.5) |
| 310 | 11 | 13:52:08 | 13:53:57 | L11 | 70 | 0 | 78.4 | 3.7 | 38 | reduced NR (96.5) |
| 311 | 10 | 13:57:17 | 13:58:45 | L10 | 90 | 0 | 78.4 | 4.2 | 347 | reduced NR (96.5) |
| 312 | 9 | 14:01:59 | 14:03:11 | L9 | 110 | 0 | 78.8 | 1.7 | 350 | reduced NR (96.5) |
| 313 | 8 | 14:06:35 | 14:07:36 | L8 | 130 | 0 | 79.6 | 0.5 | 1 | reduced NR (96.5) |
| 314 | 7 | 14:11:09 | 14:12:04 | L7 | 145 | 0 | 79.1 | 0.0 | 315 | reduced NR (96.5)--150 KTAS actual |
| 315 | 13 | 14:16:16 | 14:17:13 | A1 | 80 | 6 | 80.3 | 1.5 | 313 | headwinds aloft (ABORT: terminated at pilot discretion) |
| 316 | 13-1 | 14:20:28 | 14:21:25 | A1 | 80 | 6 | 79.5 | 3.7 | 336 | headwinds aloft |
| 317 | 14 | 14:25:43 | 14:26:43 | A2 | 80 | 6 | 79.7 | 0.0 | 342 | nose left sideslip (20°-25°) |
| 318 | 15 | 14:31:06 | 14:32:12 | A3 | 70 | 3 | 81.1 | 0.0 | 20 | |
| 319 | 16 | 14:36:18 | 14:37:20 | A4 | 70 | 6 | 80.8 | 0.5 | 264 | |
| 320 | 17 | 14:41:48 | 14:42:48 | A5 | 70 | 9 | 81.5 | 0.0 | 15 | |
| 321 | 21 | 14:46:36 | 14:47:38 | A9 | 70 | 3 | 80.9 | 1.2 | 6 | reduced NR (96.5), pilot was OK skipping 98% runs |
| 322 | 22 | 14:51:15 | 14:52:18 | A10 | 70 | 6 | 80.9 | 2.2 | 271 | reduced NR (96.5) |
| 323 | 3-2 | 14:55:52 | 14:57:05 | L3 | 110 | 0 | 81.4 | 0.7 | 350 | |
| 909 | N/A | 15:08:31 | 15:09:30 | Ambient | n/a | n/a | 82.2 | 1.7 | 8 | |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 13. UH-60M flight card for 8/6/13.

| Date: 8/6/13 | | UTC=Local + 5 hours | | | LTC Evan Brown / CW3 Clark Hall | | | | | Note: Times in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|---------------------------------|---------|-----------------------|----------|----------|---|
| Aircraft: HH-60M | | Flight Number: 105 | | | GW#: 16,600 ± 50 | | Fuel Start Wt #: 2377 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 910 | N/A | 10:15:46 | 10:16:47 | ambient | n/a | n/a | 70.5 | 0.0 | 350 | |
| 324 | 3-3 | 11:10:45 | 11:11:59 | L3 | 110 | 0 | 67.9 | 0.0 | 27 | |
| 325 | 13-2 | 11:16:01 | 11:16:57 | A1 | 80 | 6 | 68.3 | 0.0 | 27 | |
| 326 | 14-1 | 11:21:58 | 11:22:57 | A2 | 80 | 6 | 70.5 | 0.0 | 27 | nose left sideslip (~20°)-- temperature inversion (+8°F over 300') |
| 327 | 15-1 | 11:27:09 | 11:28:34 | A3 | 70 | 3 | 68.5 | 0.0 | 27 | |
| 328 | 16-1 | 11:32:32 | 11:33:34 | A4 | 70 | 6 | 68.5 | 0.0 | 27 | |
| 329 | 17-1 | 11:37:35 | 11:38:42 | A5 | 70 | 9 | 68.8 | 0.0 | 27 | |
| 330 | 15-2 | 11:42:37 | 11:43:42 | A3 | 70 | 3 | 69.3 | 0.0 | 27 | actual 100.5% |
| 331 | 16-2 | 11:47:44 | 11:48:48 | A4 | 70 | 6 | 69.6 | 0.0 | 27 | actual 100.5% |
| 332 | 23 | 11:53:47 | 11:54:54 | A11 | 70 | 9 | 69.9 | 0.0 | 27 | reduced NR (96.5%) a/c at 35,000 ft |
| 333 | 21-1 | 11:59:18 | 12:00:17 | A3 | 70 | 3 | 70.0 | 0.0 | 27 | actual 100.5% |
| 334 | 22-1 | 12:04:55 | 12:06:00 | A4 | 70 | 6 | 70.7 | 0.0 | 27 | actual 100.5% |
| 335 | 24 | 12:10:20 | 12:11:32 | A12 | 50 | 3 | 71.2 | 0.0 | 27 | |
| 336 | 25 | 12:15:48 | 12:17:06 | A13 | 50 | 6 | 72.0 | 0.0 | 27 | |
| 337 | 26 | 12:21:38 | 12:22:58 | A14 | 50 | 9 | 72.2 | 0.0 | 27 | |
| 338 | 30 | 12:27:16 | 12:28:31 | A18 | 50 | 3 | 72.7 | 1.7 | 24 | reduced NR (96.5%) |
| 339 | 31 | 12:32:58 | 12:34:21 | A19 | 50 | 6 | 73.2 | 0.0 | 6 | reduced NR (96.5%) |
| 340 | 32 | 12:38:55 | 12:40:16 | A20 | 50 | 9 | 74.0 | 0.0 | 4 | reduced NR (96.5%) |
| 341 | 3-4 | 12:44:50 | 12:47:52 | L3 | 110 | 0 | 74.6 | 0.7 | 28 | extended path |
| 342 | 36 | 12:52:07 | 12:53:25 | M1 | 70-50-0 | - | 74.9 | 0.5 | 29 | compound approach (50' high) jet overflight |
| 343 | 36-1 | 12:58:03 | 12:59:37 | M1 | 70-50-0 | - | 74.7 | 0.0 | 16 | compound approach |
| 344 | 34 | 13:00:27 | 13:02:03 | H2/H3 | 0 | 0 | 75.3 | 0.2 | 19 | NASA hover (30 sec then heading change) |
| 345 | 33 | 13:03:42 | 13:04:23 | H1 | 0 | 0 | 75.7 | 0.0 | 19 | NSWC hover |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 13. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|---|
| Refuel | | | | | | | | | | |
| 911 | N/A | 13:13:20 | 13:14:21 | ambient | n/a | n/a | 74.7 | 0.0 | 19 | |
| 346 | 3-5 | 13:52:10 | 13:54:41 | L3 | 110 | 0 | 79.3 | 0.0 | 359 | extended path (jet noise in area near beginning of run) |
| 347 | 37 | 13:58:16 | 13:59:07 | M2 | 110 | 0 | 79.9 | 0.5 | 8 | 20° bank right turn |
| 348 | 40 | 14:01:15 | 14:02:19 | M5 | 110 | 0 | 80.0 | 0.0 | 2 | 30° bank right turn |
| 349 | 6-2 | 14:05:02 | 14:07:21 | L6 | 50 | 0 | 80.6 | 0.0 | 2 | |
| 350 | 5-1 | 14:10:18 | 14:11:59 | L5 | 70 | 0 | 80.5 | 1.2 | 298 | |
| 351 | 4-1 | 14:14:59 | 14:16:15 | L4 | 90 | 0 | 80.7 | 2.4 | 332 | pickup idling near NSWC since REFUEL |
| 352 | 3-6 | 14:20:14 | 14:22:43 | L3 | 110 | 0 | 81.9 | 0.7 | 28 | extended path |
| 353 | 2-1 | 14:25:55 | 14:26:55 | L2 | 130 | 0 | 81.6 | 1.7 | 346 | |
| 354 | 1-1 | 14:34:19 | 14:35:08 | L1 | 145 | 0 | 81.5 | 2.0 | 339 | 152 KTAS actual |
| 355 | 7-1 | 14:38:08 | 14:39:02 | L7 | 145 | 0 | 81.8 | 1.2 | 7 | 150 KTAS actual, reduced NR(96.5%) |
| 356 | 8-1 | 14:42:00 | 14:43:00 | L8 | 130 | 0 | 81.7 | 1.5 | 347 | reduced NR (96.5%) |
| 357 | 9-1 | 14:45:37 | 14:46:51 | L9 | 110 | 0 | 81.6 | 2.4 | 348 | reduced NR (96.5%) |
| 358 | 10-1 | 14:49:39 | 14:51:07 | L10 | 90 | 0 | 82.8 | 0.2 | 344 | reduced NR (96.5%) |
| 359 | 11-1 | 14:53:58 | 14:55:48 | L11 | 70 | 0 | 83.3 | 0.0 | 300 | reduced NR (96.5%) |
| 360 | 12-1 | 14:58:33 | 15:01:02 | L12 | 50 | 0 | 83.0 | 2.9 | 14 | reduced NR (96.5%) |
| 912 | N/A | 15:10:31 | 15:11:31 | ambient | n/a | n/a | 82.6 | 4.9 | 31 | UH-1 inbound to C7 during ambient |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 14. HH-60M flight card for 8/7/13.

| Date: 8/7/13 | | UTC=Local + 5 hours | | | LTC Evan Brown / CW3 Clark Hall | | | | | Note: Times in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|---------------------------------|---------|-----------------------|----------|----------|---|
| Aircraft: HH-60M | | Flight Number: 106 | | | GW#: 16,600 ± 50 | | Fuel Start Wt #: 2377 | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 913 | N/A | 10:01:55 | 10:02:55 | ambient | n/a | n/a | 67.4 | 2.0 | 345 | |
| 361 | 3-7 | 11:06:28 | 11:07:53 | L3 | 110 | 0 | 67.9 | 1.2 | 17 | Microphone 14 down |
| 362 | 36-2 | 11:10:46 | 11:13:17 | M1 | 60-50-0 | - | 67.8 | 0.0 | 17 | Revised to start descent around 60 KTAS |
| 363 | 36-3 | 11:15:04 | 11:17:24 | M1 | 60-50-0 | - | 67.7 | 0.2 | 17 | Significant wind gradients (5 kts / 100', 15 kts @ 43°) |
| 364 | 36-4 | 11:18:42 | 11:21:12 | M1 | 60-50-0 | - | 67.8 | 1.7 | 17 | |
| 365 | 37-1 | 11:23:20 | 11:24:16 | M2 | 110 | 0 | 68.0 | 1.2 | 36 | GRAS 47AX O/D 20° right bank |
| 366 | 37-2 | 11:26:31 | 11:27:17 | M2 | 110 | 0 | 68.1 | 1.5 | 36 | 20° right bank |
| 367 | 37-3 | 11:29:31 | 11:30:23 | M2 | 110 | 0 | 68.3 | 0.7 | 39 | 20° right bank |
| 368 | 38 | 11:32:42 | 11:33:36 | M3 | 90 | 0 | 68.4 | 0.7 | 40 | 20° right bank, Mic 22 O/D |
| 369 | 38-1 | 11:35:58 | 11:36:49 | M3 | 90 | 0 | 68.4 | 0.0 | 41 | 20° right bank |
| 370 | 38-2 | 11:38:58 | 11:39:51 | M3 | 90 | 0 | 68.5 | 0.5 | 41 | 20° right bank |
| 371 | 39 | 11:42:05 | 11:42:57 | M4 | 70 | 0 | 68.7 | 2.4 | 2 | 20° right bank |
| 372 | 39-1 | 11:45:08 | 11:46:07 | M4 | 70 | 0 | 68.9 | 0.0 | 41 | 20° right bank |
| 373 | 39-2 | 11:48:08 | 11:49:08 | M4 | 70 | 0 | 68.8 | 0.0 | 41 | 20° right bank |
| 374 | 40-1 | 11:51:11 | 11:52:00 | M5 | 110 | 0 | 70.8 | 0.0 | 41 | 30° right bank |
| 375 | 40-2 | 11:53:54 | 15:54:44 | M5 | 110 | 0 | 68.8 | 0.7 | 41 | 30° right bank (O/D 20,21,22) |
| 376 | 40-3 | 11:56:33 | 11:57:21 | M5 | 110 | 0 | 68.9 | 0.0 | 20 | 30° right bank |
| 377 | 41 | 11:59:17 | 12:00:12 | M6 | 90 | 0 | 68.9 | 0.0 | 20 | 30° right bank |
| 378 | 41-1 | 12:02:03 | 12:02:50 | M6 | 90 | 0 | 69.2 | 0.0 | 20 | 30° right bank |
| 379 | 41-2 | 12:04:43 | 12:05:32 | M6 | 90 | 0 | 69.3 | 2.2 | 24 | 30° right bank |
| 380 | 42 | 12:07:31 | 12:08:30 | M7 | 70 | 0 | 69.2 | 1.7 | 24 | 30° right bank |
| 381 | 42-1 | 12:10:24 | 12:11:19 | M7 | 70 | 0 | 69.3 | 0.0 | 24 | 30° right bank |
| 382 | 42-2 | 12:13:12 | 12:14:06 | M7 | 70 | 0 | 69.3 | 0.0 | 24 | 30° right bank |
| 383 | 43 | 12:17:07 | 12:18:06 | M8 | 110 | 0 | 69.8 | 0.0 | 24 | 20° left bank |
| 384 | 43-1 | 12:20:17 | 12:21:16 | M8 | 110 | 0 | 69.8 | 0.2 | 20 | 20° left bank |
| 385 | 43-2 | 12:23:19 | 12:24:19 | M8 | 110 | 0 | 69.8 | 0.0 | 20 | 20° left bank |
| 386 | 44 | 12:26:25 | 12:27:26 | M9 | 90 | 0 | 69.5 | 2.7 | 10 | 20° left bank |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 14. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|--|
| 387 | 44-1 | 12:29:33 | 12:30:33 | M9 | 90 | 0 | 69.9 | 0.0 | 7 | 20° left bank |
| 388 | 44-2 | 12:32:35 | 12:33:34 | M9 | 90 | 0 | 70.1 | 0.0 | 7 | 20° left bank |
| 389 | 45 | 12:35:49 | 12:36:48 | M10 | 70 | 0 | 70.1 | 0.0 | 7 | 20° left bank |
| 390 | 45-1 | 12:39:05 | 12:40:05 | M10 | 70 | 0 | 70.3 | 0.0 | 7 | 20° left bank |
| 391 | 45-2 | 12:42:12 | 12:43:15 | M10 | 70 | 0 | 70.3 | 0.0 | 7 | 20° left bank |
| 392 | 46 | 12:45:15 | 12:46:05 | M11 | 110 | 0 | 71.6 | 0.5 | 7 | 30° left bank |
| 393 | 46-1 | 12:48:02 | 12:48:51 | M11 | 110 | 0 | 70.5 | 2.4 | 18 | 30° left bank |
| 394 | 46-2 | 12:50:48 | 12:51:37 | M11 | 110 | 0 | 70.9 | 1.0 | 19 | 30° left bank |
| 395 | 47 | 12:53:37 | 12:54:28 | M12 | 90 | 0 | 70.6 | 1.7 | 34 | 30° left bank |
| 396 | 47-1 | 12:56:20 | 12:57:11 | M12 | 90 | 0 | 71.0 | 0.7 | 27 | 30° left bank |
| 397 | 47-2 | 12:59:05 | 12:59:59 | M12 | 90 | 0 | 71.4 | 1.7 | 27 | 30° left bank |
| 398 | 3-8 | 13:01:53 | 13:02:57 | L3 | 110 | 0 | 72.7 | 0.2 | 27 | |
| Refuel | | | | | | | | | | |
| 914 | N/A | 13:16:26 | 13:17:31 | ambient | n/a | n/a | 75.0 | 2.9 | 62 | |
| 399 | 3-9 | 13:43:57 | 13:45:06 | L3 | 110 | 0 | 76.1 | 0.5 | 51 | |
| 400 | 48 | 13:47:40 | 13:48:34 | M13 | 70 | 0 | 75.6 | 2.0 | 353 | 30° left bank |
| 401 | 48-1 | 13:50:50 | 13:51:42 | M13 | 70 | 0 | 76.6 | 0.2 | 51 | 30° left bank |
| 402 | 48-2 | 13:54:14 | 13:54:58 | M13 | 70 | 0 | 76.0 | 2.0 | 53 | 30° left bank (jet noise near end of run) |
| 403 | 49 | 13:57:07 | 13:58:16 | M14 | 90-0 | 0 | 77.2 | 0.5 | 53 | quick stop |
| 404 | 49-1 | 14:00:35 | 14:01:45 | M14 | 90-0 | 0 | 77.1 | 2.9 | 92 | quick stop (decel increased at end of run) |
| 405 | 49-2 | 14:03:58 | 14:04:34 | M14 | 90-0 | 0 | 77.2 | 1.2 | 92 | quick stop (ABORT) |
| 406 | 49-3 | 14:06:59 | 14:08:33 | M14 | 90-0 | 0 | 78.9 | 0.0 | 55 | quick stop |
| 407 | 50 | 14:10:33 | 14:11:42 | M15 | 90-0 | 0 | 78.0 | 2.4 | 67 | descending quick stop |
| 408 | 50-1 | 14:13:53 | 14:15:02 | M15 | 90-0 | 0 | 77.8 | 2.2 | 67 | descending quick stop |
| 409 | 50-2 | 14:17:09 | 14:18:10 | M15 | 90-0 | 0 | 78.1 | 0.0 | 65 | |
| 410 | 51 | 14:20:35 | 14:21:45 | M16 | 90-0 | 0 | 77.8 | 2.0 | 123 | faster M14, bit unsteady |
| 411 | 51-1 | 14:23:56 | 14:25:05 | M16 | 90-0 | 0 | 77.4 | 1.7 | 123 | faster M14 |
| 412 | 51-2 | 14:27:21 | 14:28:24 | M16 | 90-0 | 0 | 77.8 | 2.9 | 116 | faster M14 |
| 413 | 1-2 | 14:31:56 | 14:32:47 | L1 | 145 | 0 | 78.2 | 0.0 | 79 | 151 KTAS actual |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 14. Concluded.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|--------------------|
| 414 | 7-2 | 14:36:30 | 14:37:22 | L7 | 145 | 0 | 80.3 | 2.0 | 126 | reduced NR (96.5%) |
| 415 | 2-2 | 14:40:50 | 14:41:46 | L2 | 130 | 0 | 80.2 | 3.2 | 53 | |
| 416 | 8-2 | 14:44:43 | 14:45:41 | L8 | 120 | 0 | 80.6 | 3.4 | 71 | reduced NR (96.5%) |
| 417 | 9-2 | 14:48:40 | 14:49:47 | L9 | 110 | 0 | 83.9 | 2.7 | 40 | reduced NR (96.5%) |
| 418 | 3-10 | 14:52:56 | 14:53:51 | L3 | 110 | 0 | 81.3 | 2.2 | 109 | |
| 419 | 4-2 | 14:56:40 | 14:57:57 | L4 | 90 | 0 | 81.4 | 8.4 | 54 | |
| 420 | 10-2 | 15:00:45 | 15:02:02 | L10 | 90 | 0 | 80.7 | 2.2 | 54 | reduced NR (96.5%) |
| 915 | N/A | 15:12:43 | 15:13:43 | ambient | n/a | n/a | 81.9 | 4.2 | 103 | |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 15. CV-22B test conditions.

| Priority | Condition Code | KCAS | Nacelle Angle, deg. | Glide slope, deg | Descent rate, fpm | Comments |
|----------|----------------|----------|---------------------|------------------|-------------------|--|
| 11 | L1 | VNE | 0 | 0 | 0 | |
| 1 | L2 | 220 | 0 | 0 | 0 | |
| 6 | L3 | 190 | 0 | 0 | 0 | |
| 7 | L4 | 160 | 0 | 0 | 0 | |
| 2 | L5 | 130 | 60 | 0 | 0 | |
| 8 | L6 | 110 | 60 | 0 | 0 | |
| 3 | L7 | 80 | 60 | 0 | 0 | |
| 4 | L8 | 70 | 87 | 0 | 0 | |
| 9 | L9 | 50 | 87 | 0 | 0 | |
| 17 | A1 | 80 | 60 | 4 | 565 | |
| 18 | A2 | 60 | 87 | 4 | 424 | |
| 12 | A3 | 80 | 60 | 7 | 987 | |
| 13 | A4 | 60 | 87 | 7 | 741 | |
| 14 | A5 | 80 | 60 | 10 | 1407 | |
| 15 | A6 | 60 | 87 | 10 | 1055 | |
| 16 | H1 | 0 | 87 | - | - | Altitude 250 feet, Heading 310°, at NSWV hover point |
| 19 | H2 | 0 | 87 | - | - | Altitude 100 feet, Heading 310°, at NASA hover point |
| 20 | H3 | 0 | 87 | - | - | Altitude 100 feet, Heading 40°, at NASA hover point |
| 10 | M1 | 200 to 0 | as req'd | as req'd | as req'd | Transition from cruise to land at approach point compressed to start at 1 mile |
| 5 | M2 | 200 to 0 | as req'd | as req'd | as req'd | Transition from cruise to land at NSWV hover point compressed to start at 1 mile |

Table 16. CV-22B flight card for 8/13/13.

| Date: 8/13/13 | | UTC=Local + 5 hours | | | Maj Dirkes / Maj McMullen | | | | | Note: Times in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|---------------------------|---------|-------------------------|----------|----------|--|
| Aircraft: CV-22B | | Flight Number: 107 | | | GW: ~47,000# | | Fuel Start Wt: ~13,000# | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 916 | N/A | 10:26:30 | 10:27:30 | ambient | n/a | n/a | | | | All level flights at 150' altitude |
| 501 | 3 | 11:36:43 | 11:37:45 | L3 | 192 | 0 | 69.3 | 0.0 | 321 | 0° nacelle (rear door open), gear up |
| 502 | 3-1 | 11:40:24 | 11:41:19 | L3 | 192 | 0 | 69.8 | 0.0 | 321 | 0° nacelle (192 KCAS), gear up |
| 503 | 1 | 11:44:44 | 11:45:28 | L1 | 267 | 0 | 70.0 | 0.0 | 321 | 0° nacelle (temp. inversion +10°F over 300') 267 KCAS actual, gear up |
| 504 | 1-1 | 11:48:11 | 11:48:53 | L1 | 265 | 0 | 69.4 | 0.0 | 321 | 0° nacelle 265 KCAS actual, gear up |
| 505 | 2 | 11:51:30 | 11:52:17 | L2 | 221 | 0 | 69.8 | 0.0 | 321 | 0° nacelle, gear up |
| 506 | 2-1 | 11:54:49 | 11:55:38 | L2 | 220 | 0 | 69.8 | 0.0 | 321 | 0° nacelle, gear up |
| 507 | 4 | 11:57:59 | 11:58:59 | L4 | 160 | 0 | 70.7 | 0.0 | 321 | 0° nacelle (160 KCAS @ 84% NR), gear up |
| 508 | 4-1 | 12:01:14 | 12:02:16 | L4 | 160 | 0 | 71.3 | 0.0 | 5 | 0° nacelle (160 KCAS @ 84% NR), gear up |
| 509 | 5 | 12:04:35 | 12:05:46 | L5 | 130 | 0 | 71.7 | 0.0 | 318 | 44° nacelle, 100% NR, Mics O/D, gear up |
| 510 | 5-1 | 12:08:28 | 12:09:42 | L5 | 130 | 0 | 72.3 | 0.0 | 318 | 44° nacelle, 100% NR, gear up |
| 511 | 5-2 | 12:12:27 | 12:13:47 | L5 | 130 | 0 | 73.1 | 0.0 | 318 | 44° nacelle, 100% NR, gear up |
| 512 | 6 | 12:16:40 | 12:17:49 | L6 | 110 | 0 | 73.6 | 0.0 | 318 | 60° nacelle, gear down |
| 513 | 6-1 | 12:20:11 | 12:21:43 | L6 | 110 | 0 | 74.2 | 0.0 | 318 | 60° nacelle, gear down |
| 514 | 7 | 12:24:46 | 12:26:45 | L7 | 80 | 0 | 74.8 | 0.0 | 318 | 79° nacelle, 100% NR, gear down |
| 515 | 7-1 | 12:29:22 | 12:31:27 | L7 | 80 | 0 | 74.6 | 0.0 | 322 | 79° nacelle, 100% NR, gear down |
| 516 | 8 | 12:34:27 | 12:36:37 | L8 | 74 var | 0 | 74.8 | 0.0 | 293 | 81° nacelle, 100% NR, gear down, A/S fluctuated |
| 517 | 8-1 | 12:39:03 | 12:41:19 | L8 | 70 | 0 | 75.5 | 0.0 | 293 | 81° nacelle, 100% NR, gear down |
| 518 | 8-2 | 12:43:38 | 12:45:48 | L8 | 70 | 0 | 75.7 | 0.0 | 293 | 81° nacelle, 100% NR, gear down |
| 519 | 9 | 12:48:29 | 12:51:38 | L9 | 50 | 0 | 76.5 | 2.2 | 297 | 85° nacelle, 104% NR, gear down |
| 520 | 9-1 | 12:54:47 | 12:57:35 | L9 | 50 | 0 | 77.6 | 0.0 | 300 | 85° nacelle, 104% NR, gear down, ±3 kts A/S |
| 521 | 3-2 | 13:00:00 | 13:00:53 | L3 | 190 | 0 | 78.6 | 0.5 | 288 | 0° nacelle, 84% NR, gear up |
| 522 | 10 | 13:04:47 | 13:06:32 | A1 | 80 | 4 | 78.3 | 3.2 | 274 | 80° nacelle, steeper approach near beginning of run (15 kts headwind @ 300') |
| 523 | 10-1 | 13:09:35 | 13:11:39 | A1 | 80±3 | 4 | 78.1 | 4.9 | 270 | 80° nacelle, ±3 kts A/S |
| 524 | 10-2 | 13:14:42 | 13:16:46 | A1 | 80±3 | 4 | 77.5 | 2.2 | 276 | 80° nacelle, ±3 kts A/S |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 16. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|-------|---------|-----------|----------|----------|--|
| 525 | 11 | 13:19:28 | 13:21:58 | A2 | 60±3 | 4 | 78.0 | 1.2 | 274 | 104% NR for a little bit at beginning, 80° nacelle, ±3 kts A/S |
| 526 | 11-1 | 13:25:15 | 13:27:48 | A2 | 60±3 | 4 | 78.3 | 0.0 | 267 | 83° nacelle, ±3 A/S |
| 527 | 12 | 13:30:46 | 13:32:49 | A3 | 80 | 7 | 78.5 | 3.9 | 319 | 78° nacelle |
| 528 | 12-1 | 13:35:46 | 13:37:44 | A3 | 80 | 7 | 78.7 | 2.9 | 295 | 78° nacelle |
| 529 | 13 | 13:40:46 | 13:43:11 | A4 | 60±3 | 7 | 78.9 | 4.4 | 269 | 82° nacelle (bit shallow) |
| 530 | 13-1 | 13:45:52 | 13:48:29 | A4 | 60±3 | 7 | 78.8 | 4.4 | 261 | 82° nacelle |
| 531 | 14 | 13:52:06 | 13:54:10 | A5 | 80±5 | 10 | 79.1 | 1.0 | 281 | 80° nacelle |
| 532 | 3-3 | 13:56:51 | 13:57:41 | L3 | 190 | 0 | 78.4 | 3.2 | 250 | balloon wind direction stuck since morning |
| 533 | 17 | 14:01:18 | 14:03:06 | H2-H3 | 0 | 0 | 78.5 | 4.6 | 279 | NASA hover |
| 534 | 16 | 14:05:52 | 14:06:43 | H1 | 0 | 0 | 78.9 | 4.9 | 255 | NSWC hover, O/D some mics |
| 535 | 19 | 14:09:37 | 14:11:13 | M1 | 200-0 | - | 79.5 | 4.3 | 253 | overshot PMA, slight O/D |
| 536 | 19-1 | 14:13:56 | 14:15:01 | M1 | 170-0 | - | 79.5 | 4.9 | 316 | 170 KCAS entry |
| 537 | 19-2 | 14:18:15 | 14:19:14 | M1 | 170-0 | - | 80.4 | 2.4 | 298 | |
| 538 | 20 | 14:23:10 | 14:23:44 | M2 | 170-0 | - | 81.6 | 1.5 | 287 | 170 KCAS entry (abort) |
| 539 | 20-1 | 14:26:29 | 14:27:36 | M2 | 170-0 | 0 | 80.9 | 6.6 | 295 | level decel from 170 KCAS (O/D on SMA) |
| 540 | 20-2 | 14:30:17 | 14:31:22 | M2 | 170-0 | 0 | 80.8 | 8.6 | 302 | |
| 541 | 14-1 | 14:34:43 | 14:36:57 | A5 | 80±5 | 10 | 80.9 | 5.1 | 303 | 80° nacelle |
| 542 | 3-4 | 14:39:13 | 14:40:12 | L3 | 190 | 0 | 80.8 | 8.3 | 332 | |
| 917 | N/A | 14:43:46 | 14:44:57 | ambient | n/a | n/a | 81.4 | 6.4 | 299 | range quiet after 10 sec |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 17. CV-22B flight card for 8/14/13.

| Date: 8/14/13 | | UTC=Local + 5 hours | | | Maj Dirkes / Maj McMullen | | | | | Note: Times in UTC-0 |
|------------------|-------------|---------------------|---------------|------------------|---------------------------|---------|-------------------------|----------|----------|------------------------------|
| Aircraft: CV-22B | | Flight Number: 108 | | | GW: ~47,000# | | Fuel Start Wt: ~13,000# | | | |
| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
| 918 | N/A | 10:19:24 | 10:20:24 | ambient | n/a | n/a | 70.7 | 0.0 | 313 | thunder during ambient? |
| 544 | 3-5 | 11:27:43 | 11:28:33 | L3 | 190 | 0 | 68.5 | 0.0 | 314 | 84% NR |
| 545 | 10.1 | 11:31:21 | 11:33:22 | A1.1 | 80 | 4 | 68.5 | 0.7 | 314 | 60° nacelle (deck not level) |
| 546 | 11-2 | 11:36:58 | 11:39:33 | A2 | 60 | 4 | 68.9 | 0.5 | 315 | level deck |
| 547 | 10-2 | 11:42:21 | 11:44:11 | A1 | 80 | 4 | 69.6 | 0.0 | 315 | 78° nacelle (level deck) |
| 548 | 12-2 | 11:47:03 | 11:49:07 | A3 | 80 | 7 | 69.9 | 0.0 | 315 | 79° nacelle (level deck) |
| 549 | 12.1 | 11:52:13 | 11:54:08 | A3.1 | 80 | 7 | 69.7 | 0.0 | 315 | 70° nacelle (deck not level) |
| 550 | 12.2 | 11:57:22 | 11:59:18 | A3.2 | 80 | 7 | 69.7 | 0.2 | 326 | 60° nacelle (deck not level) |
| 551 | 13-2 | 12:02:18 | 12:04:45 | A4 | 60 | 7 | 70.2 | 0.0 | 339 | 83° nacelle (level deck) |
| 552 | 14-2 | 12:07:12 | 12:09:13 | A5 | 80 | 10 | 70.4 | 0.0 | 340 | 80° nacelle (level deck) |
| 553 | 14.1 | 12:12:20 | 12:14:16 | A5.1 | 80 | 10 | 70.1 | 0.0 | 340 | 70° nacelle (deck not level) |
| 554 | 14.2 | 12:17:18 | 12:19:35 | A5.2 | 80 | 10 | 69.7 | 2.7 | 340 | 62° nacelle (deck not level) |
| 555 | 15 | 12:22:27 | 12:25:07 | A6 | 60 | 10 | 69.9 | 0.0 | 340 | 83° nacelle (level deck) |
| 556 | 19-3 | 12:28:02 | 12:29:11 | M1 | - | - | 70.1 | 0.0 | 340 | |
| 557 | 19-4 | 12:33:24 | 12:35:03 | M1 | - | - | 70.6 | 0.0 | 340 | |
| 558 | 20-3 | 12:37:49 | 12:38:54 | M2 | - | - | 70.7 | 0.0 | 340 | Mic O/D on SMA, center PMA |
| 559 | 20-4 | 12:41:52 | 12:43:00 | M2 | - | - | 70.9 | 0.0 | 340 | Starting at 180 KCAS |
| 560 | 1-2 | 12:46:18 | 12:47:00 | L1 | VH | 0 | 71.0 | 1.0 | 343 | 265 KCAS actual |
| 561 | 2-2 | 12:49:14 | 12:49:58 | L2 | 220 | 0 | 71.6 | 0.0 | 343 | |
| 562 | 3-5 | 12:52:11 | 12:53:02 | L3 | 190 | 0 | 71.5 | 0.0 | 343 | |
| 563 | 4.2 | 12:55:19 | 12:56:15 | L4.2 | 160 | 0 | 71.4 | 1.2 | 300 | 100% NR |
| 564 | 4-2 | 12:58:16 | 12:59:13 | L4 | 160 | 0 | 71.4 | 1.0 | 209 | back to 84% NR for A/C mode |
| 565 | 4.1 | 13:01:36 | 13:02:32 | L4.1 | 150 | 0 | 71.4 | 0.0 | 323 | |
| 566 | 5-3 | 13:05:12 | 13:06:22 | L5 | 130 | 0 | 71.6 | 4.9 | 237 | 30° nacelle |
| 567 | 6-2 | 13:08:38 | 13:10:05 | L6 | 110 | 0 | 72.0 | 0.0 | 308 | 60° nacelle |
| 568 | 6.1 | 13:12:53 | 13:14:04 | L6.1 | 110 | 0 | 72.0 | 0.0 | 308 | 50° nacelle (deck not level) |
| 569 | 7-2 | 13:16:42 | 13:18:23 | L7 | 80 | 0 | 72.1 | 0.0 | 308 | 79° nacelle (level deck) |
| 570 | 8-3 | 13:21:17 | 13:23:06 | L8 | 70 | 0 | 72.3 | 0.0 | 309 | |
| 571 | 9-2 | 13:26:03 | 13:28:33 | L9 | 50 | 0 | 72.6 | 0.0 | 309 | 85° nacelle, 104% NR |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.

Table 17. Continued.

| NASA Run # | Eglin Run # | Data On Time | Data Off Time | Flight Condition | KCAS | FPA (°) | Temp (°F) | WS (kts) | WD (deg) | Comments |
|------------|-------------|--------------|---------------|------------------|------|---------|-----------|----------|----------|---|
| 572 | 10-3 | 13:31:31 | 13:33:17 | A1 | 80 | 4 | 73.7 | 0.7 | 345 | 80° nacelle (level deck) |
| 573 | 11-3 | 13:36:37 | 13:39:01 | A2 | 60 | 4 | 74.4 | 0.0 | 345 | 83° nacelle (level deck) |
| 574 | 12-3 | 13:41:49 | 13:43:35 | A3 | 80 | 7 | 75.1 | 1.5 | 347 | 78° nacelle (level deck) |
| 575 | 13-3 | 13:46:15 | 13:48:40 | A4 | 60 | 7 | 74.8 | 2.0 | 2 | jet noise in area, 83° nacelle |
| 576 | 13-4 | 13:51:30 | 13:53:46 | A4 | 60 | 7 | 75.4 | 0.0 | 334 | 82° nacelle (level deck), still jet noise |
| 577 | 14-3 | 14:00:29 | 14:02:30 | A5 | 80 | 10 | 77.3 | 0.5 | 351 | 80° nacelle (deck level), jet noise |
| 578 | 14-4 | 14:06:05 | 14:08:02 | A5 | 80 | 10 | 78.4 | 2.2 | 19 | 79° nacelle (level deck) |
| 579 | 15-1 | 14:10:52 | 14:13:21 | A6 | 60 | 10 | 77.2 | 1.0 | 281 | 83° nacelle (level deck, shift to 104% NR after recovery) |
| 580 | 14.1-1 | 14:16:18 | 14:18:08 | A5.1 | 80 | 10 | 76.8 | 1.7 | 261 | 70° nacelle (deck not level) |
| 581 | 14.2-1 | 14:21:00 | 14:23:01 | A5.2 | 80 | 10 | 76.8 | 1.7 | 306 | 63° nacelle (deck not level) |
| 582 | 6-3 | 14:26:39 | 14:29:09 | L6 | 110 | 0 | 76.9 | 4.4 | 321 | 60° nacelle, extended run-in, some jet noise |
| 583 | 1-3 | 14:32:11 | 14:32:54 | L1 | VH | 0 | 77.6 | 1.0 | 262 | 270 KCAS actual (rear door closed) |
| 584 | 3-6 | 14:35:59 | 14:36:56 | L3 | 190 | 0 | 78.7 | 2.2 | 267 | |
| 919 | N/A | 14:46:58 | 14:47:57 | ambient | n/a | n/a | 77.8 | 3.7 | 287 | |

Footnote: ‘-’ in KCAS or FPA indicates flight speed or path angle was “as required”. See description of test conditions for more information.



Figure 1. AH-64D Apache Helicopter.



Figure 2. HH-60M Blackhawk Helicopter.



Figure 3. CV-22B Tiltrotor Aircraft.

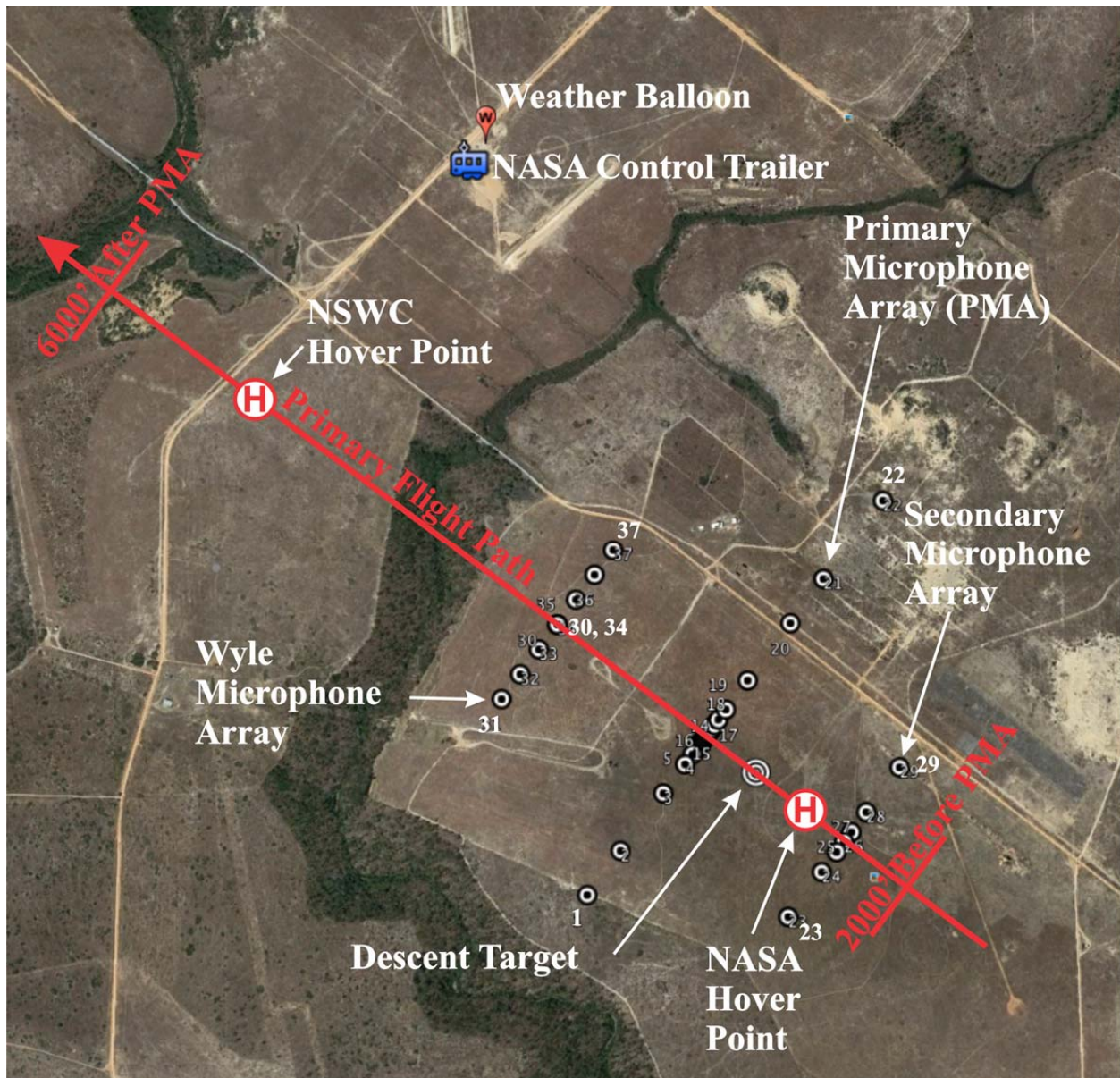


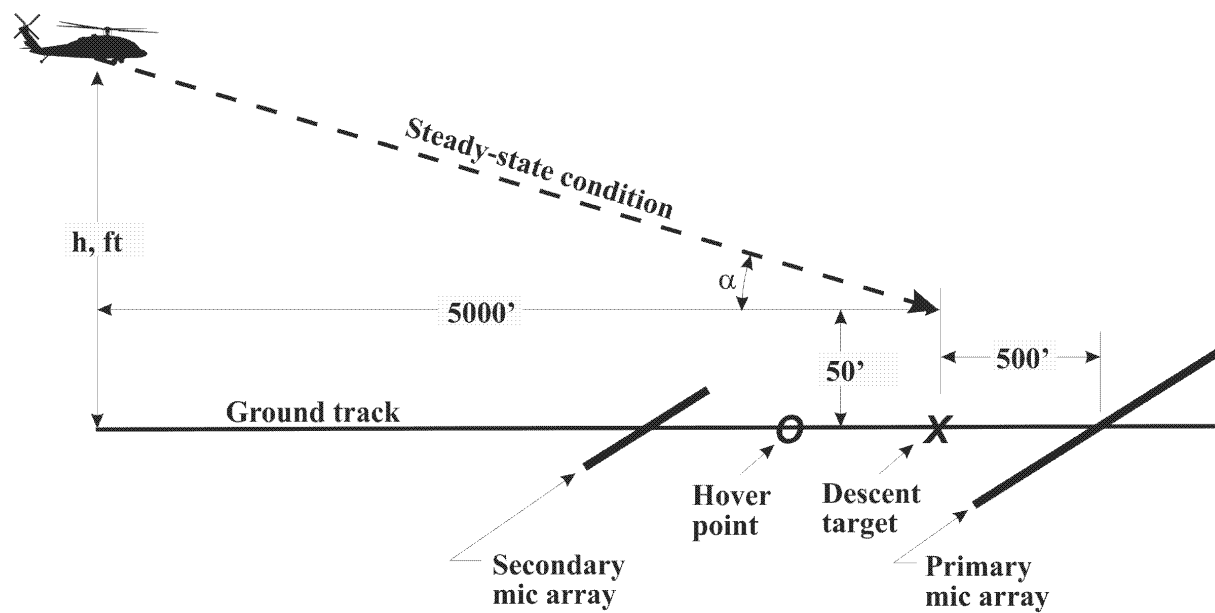
Figure 4. Test range overview.



Figure 5. Typical WAMS microphone station deployment.



Figure 6. Tethered weather balloon system.



| Descent Angle, deg | h @ 5000' out | h at 6000' out | h at 7000' out |
|--------------------|---------------|----------------|----------------|
| 3 | 312 | 364 | 417 |
| 4 | 400 | 470 | 539 |
| 6 | 576 | 681 | 786 |
| 7 | 664 | 787 | 910 |
| 9 | 842 | 1000 | 1159 |
| 10 | 932 | 1108 | 1284 |

Figure 7. Approach profile graphic with glideslope intercept altitudes.

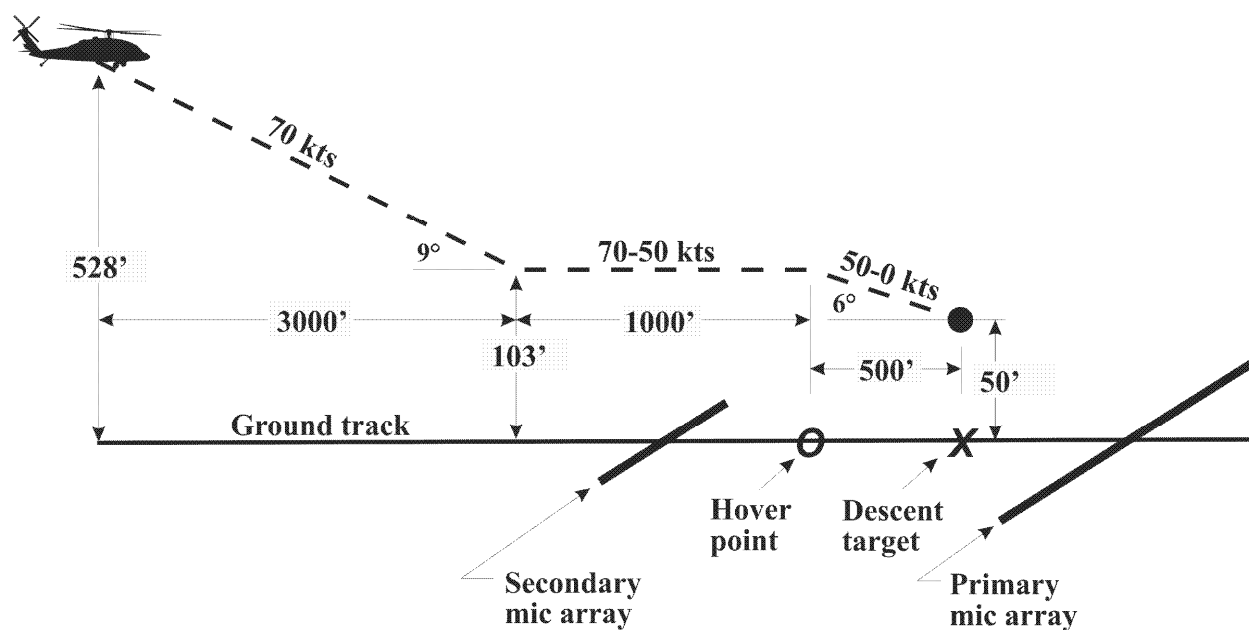


Figure 8. HH-60M descent maneuver M1 graphic.